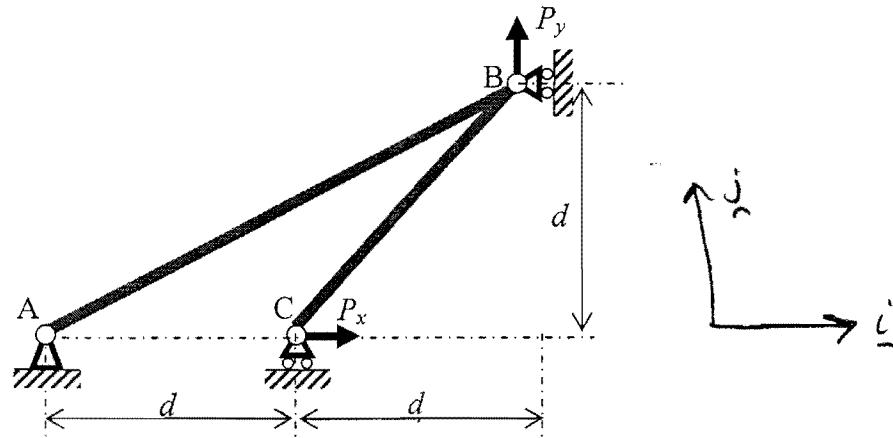


1. A truss is shown below. Both members have identical values of E and A . Joint A is pinned and joints A and C are on roller supports.



a. Is this truss statically determinate, indeterminate, or a mechanism? Why?

$$M = 2 \quad J = 3 \quad R = 4 \quad M + J = 2R \quad \text{stat det}$$

b. Determine the elongation of each member as functions of the nonzero displacement components of joints B and C. Assume small deflections.

$$\delta^{AB} = (\underline{u}^B - \underline{u}^A) \cdot \underline{n}^{AB} \quad \delta^{BC} = (\underline{u}^C - \underline{u}^B) \cdot \underline{n}^{BC}$$

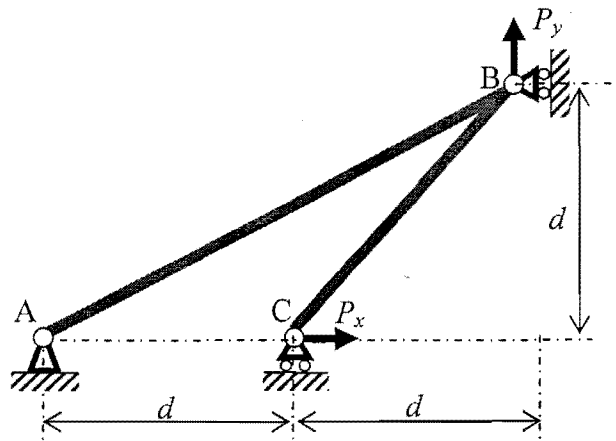
$$\underline{n}^{AB} = \frac{1}{\sqrt{5}d} (2d\underline{i} + d\underline{j}) = \frac{1}{\sqrt{5}} (2\underline{i} + \underline{j}) \quad (L_0^{AB} = \sqrt{5}d)$$

$$\underline{u}^A = \underline{0} \quad \underline{u}^B = u_y^B \underline{j} \quad (u_x^B = 0)$$

$$\Rightarrow \delta^{AB} = u_y^B \underline{j} \cdot \frac{1}{\sqrt{5}} (2\underline{i} + \underline{j}) = \frac{1}{\sqrt{5}} u_y^B = \delta^{AB}$$

$$\underline{n}^{BC} = \frac{1}{\sqrt{2}} (-\underline{i} - \underline{j}) \quad \underline{u}^C = u_x^C \underline{i} \quad (L_0^{BC} = \sqrt{2}d)$$

$$\delta^{BC} = (u_x^C \underline{i} - u_y^B \underline{j}) \cdot \frac{1}{\sqrt{2}} (-\underline{i} - \underline{j}) = \frac{1}{\sqrt{2}} (-u_x^C + u_y^B) = \delta^{BC}$$



c. Find the stiffness matrix for the structure. $V \ll PE$

$$PE: \quad V = \frac{1}{2} \frac{EA}{\sqrt{5}d} (\delta^{AB})^2 + \frac{1}{2} \frac{EA}{\sqrt{2}d} (\delta^{BC})^2 - P_x u_x^C - P_y u_y^B$$

δ^{AB} & δ^{BC} given in the previous problem

$$V = \frac{1}{2} \frac{EA}{5\sqrt{5}d} (u_y^B)^2 + \frac{1}{2} \frac{EA}{2\sqrt{2}d} (u_y^B - u_x^C)^2 - P_x u_x^C - P_y u_y^B$$

joint displacements

d. Determine the deflections and member forces for the case in which $P_x=0$. The answers will involve P_y , EA , and d .

Use Maple to solve: $\frac{\partial V}{\partial u_x^C} = 0$ $\frac{\partial V}{\partial u_y^B} = 0$

$$P_x = 0 \quad \text{Maple gives} \quad u_x^C = u_y^B = \frac{5\sqrt{5}d}{EA} P_y$$

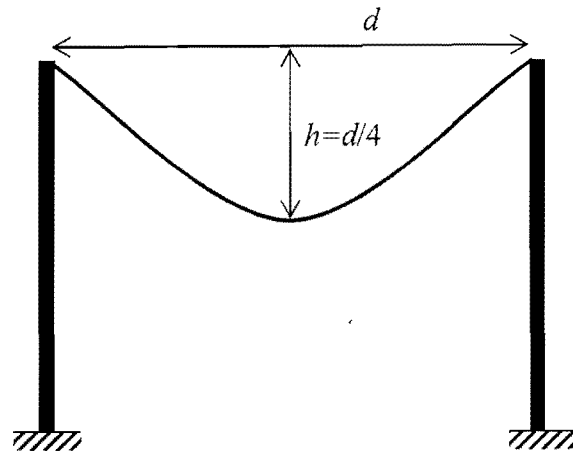
$$\delta^{AB} = \frac{1}{\sqrt{5}} u_y^B = \frac{5d}{EA} P_y$$

$$F^{AB} = \frac{EA}{\sqrt{5}d} \delta^{AB} = \frac{EA}{\sqrt{5}d} \frac{5d}{EA} P_y = \underline{\underline{\sqrt{5} P_y}}$$

$$\delta^{BC} = \frac{1}{\sqrt{2}} (u_y^B - u_x^C) = 0 \quad \underline{\underline{F^{BC} = 0}}$$

2. A uniform, inextensible transmission cable hangs under its own weight. Cable weight per unit length is w . The desired sag is equal to $d/4$.

a. Find the cable length required, and the maximum tension T_0 in the cables



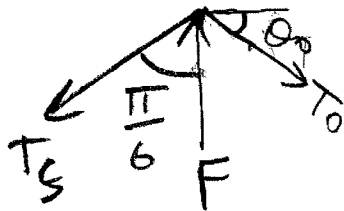
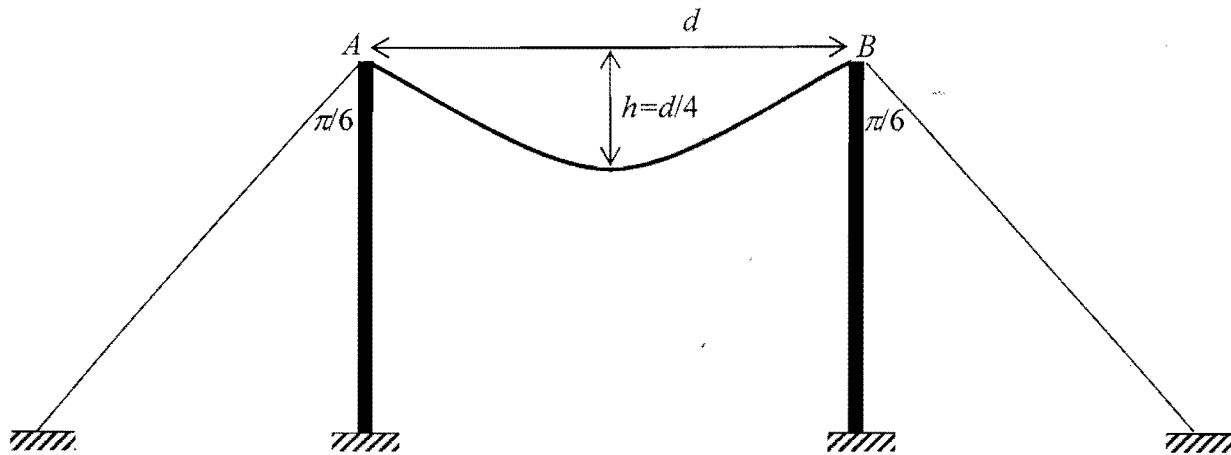
$$L_0/d = \frac{1}{c} \sinh c \quad \frac{h}{d} = \frac{1}{2c} (\cosh c - 1) \quad T_0 = \frac{wd}{2c} \cosh c$$

$$\frac{h}{d} = \frac{1}{4} = \frac{1}{2c} (\cosh c - 1) \Rightarrow \underline{c = 0.931}$$

$$\Rightarrow \underline{L_0/d = 1.151}$$

$$\underline{T_0 = 0.787 wd}$$

b. To avoid bending in the poles, support cables are added as shown to ensure that **the poles carry only axial load**. Determine the tension T_s of the support cables and the resulting compressive force F in the poles. To do this, begin with a free body diagram of the point A at the top of the left-hand pole.



$$\theta_0 = \tan^{-1}(y'/a) = \tan^{-1}(\sinh c) = 0.82 \text{ radians}$$

$$\sum F_x = 0 \quad T_0 \cos \theta_0 = T_s \sin \frac{\pi}{6}$$

$$T_s = 1.07 wd$$

$$\sum F_y = 0 \Rightarrow F = T_0 \sin \theta_0 + T_s \cos \frac{\pi}{6}$$

$$F = 1.51 wd$$