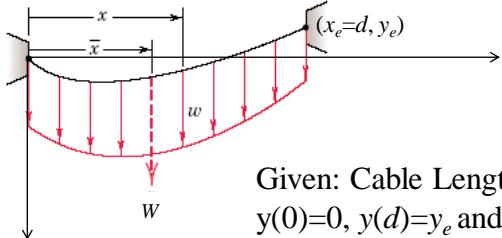
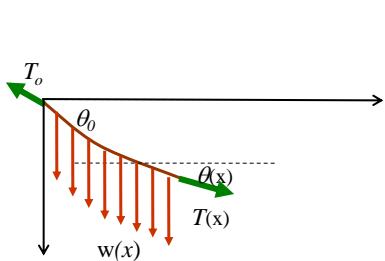


Cable Equations:



$$\frac{d^2y}{dx^2} = -\frac{w}{R_x}$$

Given: Cable Length L_0 , span d Endpoints
 $y(0)=0, y(d)=y_e$ and force $w(x)$, find $y(x)$ and R_x .



$$L_0 = \int_0^d \sqrt{1 + \left(\frac{dy}{dx}\right)^2} dx$$

$$T(x) = \frac{R_x}{\cos \theta(x)} = R_x \sqrt{1 + \left(\frac{dy}{dx}\right)^2}$$

$$\theta(x) = \tan^{-1} \frac{dy}{dx}(x)$$

Cable Under Its Own Weight

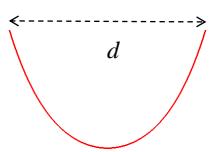
ω : weight per unit length of cable.

$$\frac{d^2y}{dx^2} = -\frac{w}{R_x} = -\frac{\omega}{R_x} \sqrt{1 + \left(\frac{dy}{dx}\right)^2}$$

$$y(x) = \frac{R_x}{\omega} \left\{ \cosh(c) - \cosh \left(c - \frac{\omega}{R_x} x \right) \right\}$$

Constants c and R_x come from $y(d)=y_e$ and

$$L_0 = \int_0^d \sqrt{1 + \left(\frac{dy}{dx}\right)^2} dx$$



Example: $y(d)=0$

$$\Rightarrow \cosh(c) = \cosh\left(c - \frac{\omega}{R_x} d\right) \Rightarrow c = \frac{\omega}{2R_x} d.$$

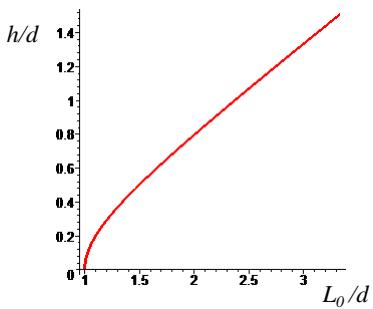
$$y(x)/d = \frac{1}{2c} \{ \cosh(c) - \cosh(c(1 - 2x/d)) \}$$

Determine the remaining constant: c

$$y(x)/d = \frac{1}{2c} \{ \cosh(c) - \cosh(c(1 - 2x/d)) \}$$

$$L_0 = \int_0^d \sqrt{1 + \left(\frac{dy}{dx}\right)^2} dx = \int_0^d \cosh(c(1 - 2x/d)) dx = \frac{d}{c} \sinh(c)$$

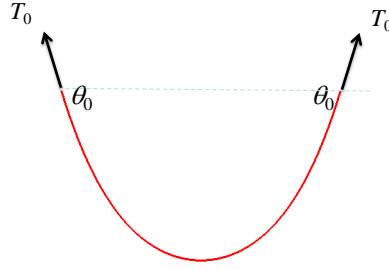
$$\Rightarrow L_0/d = \frac{1}{c} \sinh c$$



$$y(d/2) = h = \frac{d}{2c} \{ \cosh(c) - 1 \}$$

$$\Rightarrow \frac{h}{d} = \frac{1}{2c} \{ \cosh(c) - 1 \}$$

End Tension



$$2T_0 \sin \theta_0 = wL_0$$

$$\tan \theta_0 = y'(0) = \sinh(c)$$

$$\sin \theta_0 = \tanh(c) \quad T_0 = \frac{wL_0}{2 \sin \theta_0} = \frac{wL_0}{2 \tanh(c)} = \frac{wd}{2c} \cosh(c)$$

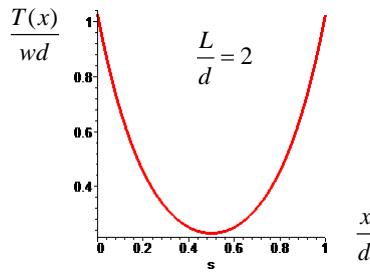
$$L_0 / d = \frac{1}{c} \sinh c$$

Internal tension

$$T(x) = T_0 \frac{\cos \theta_0}{\cos \theta(x)} = T_0 \cos \theta_0 \sqrt{1 + \tan^2 \theta(x)} = T_0 \cos \theta_0 \sqrt{1 + \left(\frac{dy}{dx} \right)^2}$$

$$T(x) = \frac{wd}{2c} \sqrt{1 + \left(\frac{dy}{dx} \right)^2}$$

$$\Rightarrow \frac{T(x)}{wd} = \frac{1}{2c} \cosh \left(c \left(1 - \frac{2x}{d} \right) \right)$$



Summary

Diagram showing a red catenary curve. A horizontal dashed line at height h from the x-axis has a double-headed arrow labeled d above it. A vertical dashed line from the vertex of the curve to the x-axis is labeled h . The width of the curve at height h is labeled d .

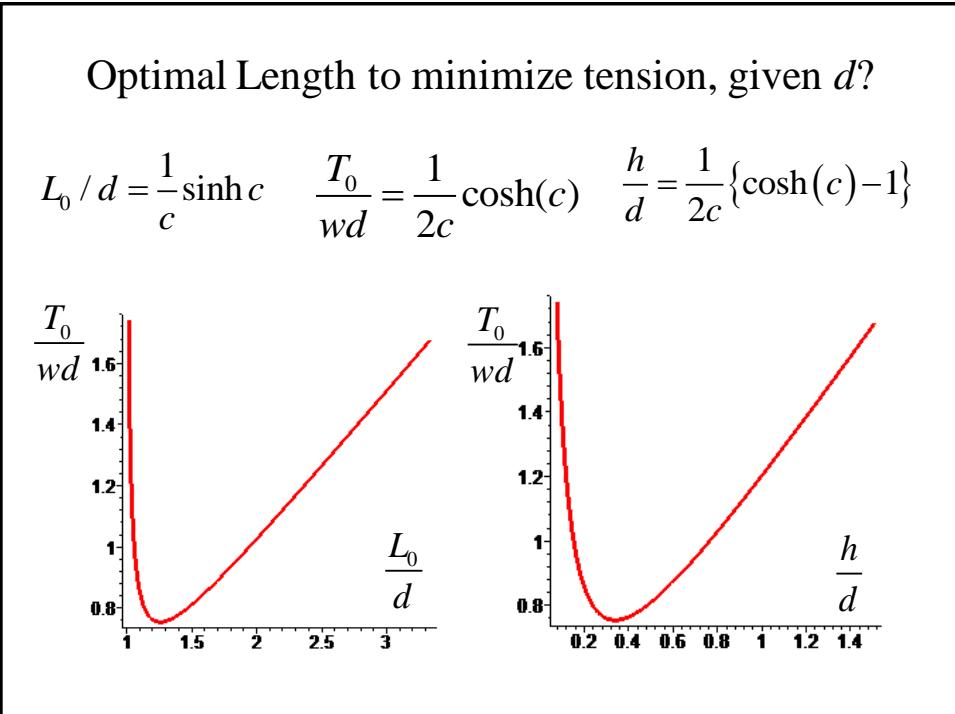
$$L_0 / d = \frac{1}{c} \sinh c$$

Get c from one of these

$$\frac{h}{d} = \frac{1}{2c} \{ \cosh(c) - 1 \}$$

$$y(x) / d = \frac{1}{2c} \{ \cosh(c) - \cosh(c(1 - 2x/d)) \}$$

$$\frac{T_0}{wd} = \frac{1}{2c} \cosh(c(1 - 2x/d))$$

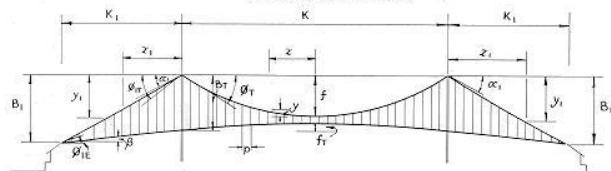
$$\frac{T(x)}{wd} = \frac{1}{2c} \cosh(c(1 - 2x/d))$$


Optimum sag is about 1/3 of the span



1930's

**Approximate Formulas for Determining Cable and Suspender Lengths
and Cable Tensions**



w = Dead load total weight per foot, including cable and suspenders.

V = Vertical component of cable tension.

H = Horizontal component of cable tension.

T = Cable tension.

phi = Angle with horizontal of tangent to cable curve.

alpha = Angle with horizontal of chord line joining ends of span.

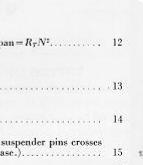
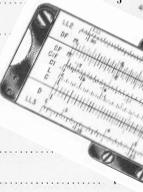
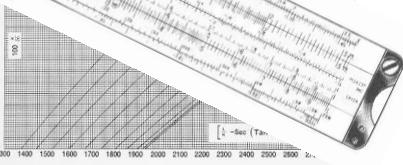
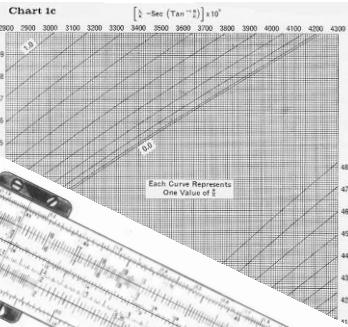
$$n = \frac{f}{K}, n_1 = \frac{f_1}{K_1} \quad (\text{sag ratio}).$$

L = Length of cable in main span.

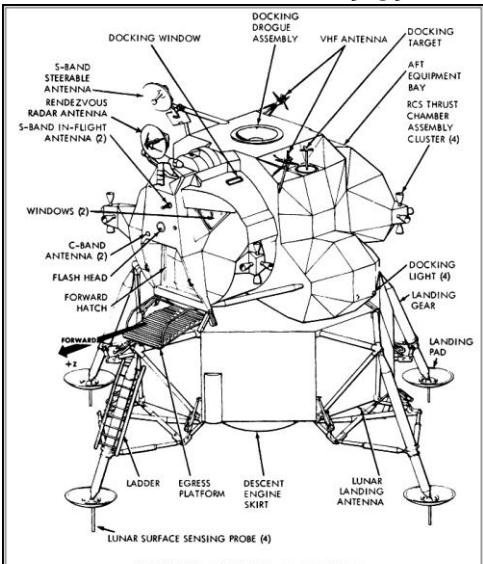
L_1 = Length of cable in side span.

Slide Rules Rule!

$H \text{ (at dead load)} = \frac{wK^2}{8f} = \frac{wK_1^2}{8f_1}$	1
$\tan \phi \text{ (at any point in main span)} = \frac{8fx}{K^2}$	2
$\tan \phi_1 \text{ (at any point in side span)} = \frac{4f_1}{K_1^2}(K_1 - 2x_1) + \frac{B_1}{K_1}$	3
$\tan \phi_T = \frac{M}{K} = 4n$	4
$\tan \phi_{T1} = \frac{B_1 + 4f_1}{K_1} = \tan \alpha_1 - 4n_1 = \tan \alpha_1 + \frac{wK_1}{2H}$	5
$\tan \phi_{T2} = \frac{B_1 - 4f_1}{K_1} = \tan \alpha_1 - 4n_1 = \tan \alpha_1 - \frac{wK_1}{2H}$	
$V = H \tan \phi$	
$T = H \sec \phi$ (see $\phi = \sqrt{1 + \tan^2 \phi}$)	
$L = K(1 + \frac{8}{3}n^2)$	
$L_1 = K \left(\sec \alpha_1 + \frac{3^2 n_1^2}{\sec \alpha_1} \right)$	
$y = \frac{4fp^2}{K^2} = RN^2$ (Where N = Number of panels from mid-span to point x)	
And $R = \frac{4fp^2}{K^2}$	
$y_T = \text{Main span truss ordinate measured down from high point at mid-span} = R_T N^2$ (Where $R_T = \frac{4fp_T^2}{K^2}$)	12
Main span suspender length = $x + y_T + S$ (Where S = Length of shortest suspender at mid-span.)	13
$y_1 = 4f_1 \left(\frac{x_1}{K_1} \left(1 - \frac{x_1}{K_1} \right) + x_1 \tan \alpha_1 \right)$	14
$y_{T1} = \text{Side span truss ordinate measured down from point where line of suspender pins crosses}\ \frac{\pi}{4} \text{ tower} = x_1 \tan \beta$. (Where side span truss is straight—the usual case.)	15
Side span suspender length = $B_T + y_{T1} - y_1$ (Where B_T = Difference in elevation between P.I. of cable saddle and line of suspender pins at $\frac{\pi}{4}$ tower.)	16
When side span is free, consider cable length a straight line, in which case $L_1 = K_1 \sec \alpha_1$	17



1969



APOLLO LUNAR MODULE