

Review

Viscous fluid in cylindrical shear cell

Velocity gradient $\mathbf{L} = \nabla_{\mathbf{y}} \mathbf{v} = \frac{\partial v_{\theta}}{\partial r} \mathbf{e}_{\theta} \otimes \mathbf{e}_r - \frac{v_{\theta}}{r} \mathbf{e}_r \otimes \mathbf{e}_{\theta}$

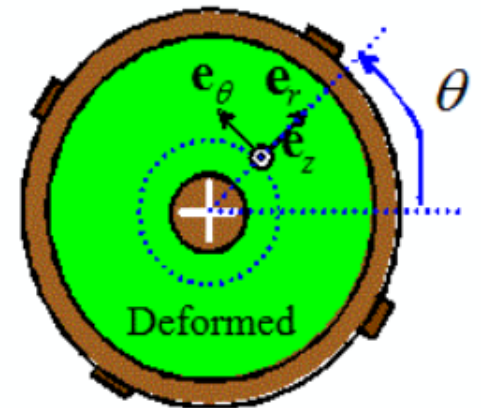
Stretch rate $\mathbf{D} = \text{sym}(\mathbf{L}) = \frac{1}{2} \left(\frac{\partial v_{\theta}}{\partial r} - \frac{v_{\theta}}{r} \right) (\mathbf{e}_{\theta} \otimes \mathbf{e}_r + \mathbf{e}_r \otimes \mathbf{e}_{\theta})$

Acceleration $\mathbf{a} = \frac{\partial \mathbf{v}}{\partial t} \Big|_{\mathbf{y}} + \mathbf{L} \mathbf{v} = -\frac{v^2}{r} \mathbf{e}_r$

Stress $\boldsymbol{\tau} = \boldsymbol{\sigma} = 2\mu \mathbf{D} + p\mathbf{I} = \mu \left(\frac{\partial v_{\theta}}{\partial r} - \frac{v_{\theta}}{r} \right) (\mathbf{e}_{\theta} \otimes \mathbf{e}_r + \mathbf{e}_r \otimes \mathbf{e}_{\theta}) + p\mathbf{I}$

Linear Momentum $\nabla_{\mathbf{y}} \cdot \boldsymbol{\sigma} = \rho \mathbf{a} = \mu \frac{\partial}{\partial r} \left(\frac{\partial v_{\theta}}{\partial r} - \frac{v_{\theta}}{r} \right) \mathbf{e}_{\theta} + 2\mu \left(\frac{\partial v_{\theta}}{\partial r} - \frac{v_{\theta}}{r} \right) \mathbf{e}_{\theta} + \frac{\partial p}{\partial r} \mathbf{e}_r = -\rho \frac{v^2}{r} \mathbf{e}_r$

Solve, with BCs $\mathbf{v}(a_0) = 0 \quad \mathbf{v}(a_1) = a_1 \omega \mathbf{e}_{\theta}$



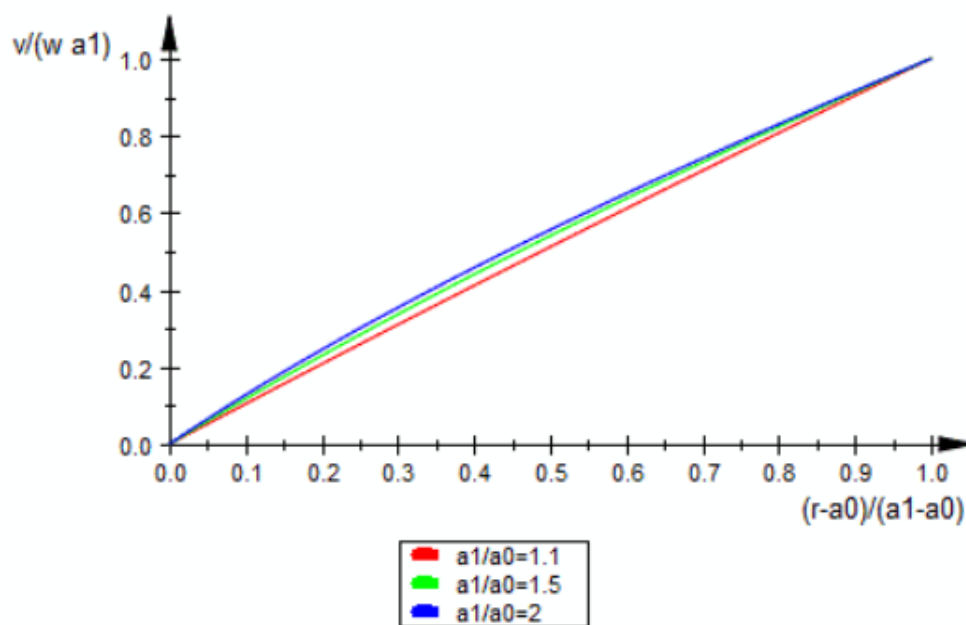
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diffeq1 := diff(diff(vq(r),r),r) + diff(vq(r),r)/r - vq(r)/r^2=0:
bc := vq(a0)=0,vq(a1)=a1*w:
vqsol := simplify(solve(ode({diffeq1,bc}, vq(r)),IgnoreSpecialCases))[1]

$$\frac{a_1^2 w (a_0^2 - r^2)}{r (a_0^2 - a_1^2)}$$

vqnorm := subs(vqsol/a1,{a0=1,w=1,r=1+(a1-1)*xi}):
plot(
plot::Function2d(subs(vqnorm,a1=1.1),xi=0..1,Color=RGB::Red,Legend="a1/a0=1.1"),
plot::Function2d(subs(vqnorm,a1=1.5),xi=0..1,Color=RGB::Green,Legend="a1/a0=1.5"),
plot::Function2d(subs(vqnorm,a1=2),xi=0..1,Color=RGB::Blue,Legend="a1/a0=2"),
AxesTitles = ["(r-a0)/(a1-a0)","v/(w a1)"]
)

```



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diffeq2 := diff(p(r),r) = -rho*vqsol^2/r:
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psol := simplify(solve(ode({diffeq2}, p(r)),IgnoreSpecialCases))[1]
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$$C5 + \frac{a1^4 \rho w^2 (a0^4 - r^4 + 4 a0^2 r^2 \ln(r))}{2 r^2 (a0^2 - a1^2)^2}$$

```
pnorm := subs(psol,{C5=0,rho=1,a0=1,w=1,r=1+(a1-1)*xi}):
```

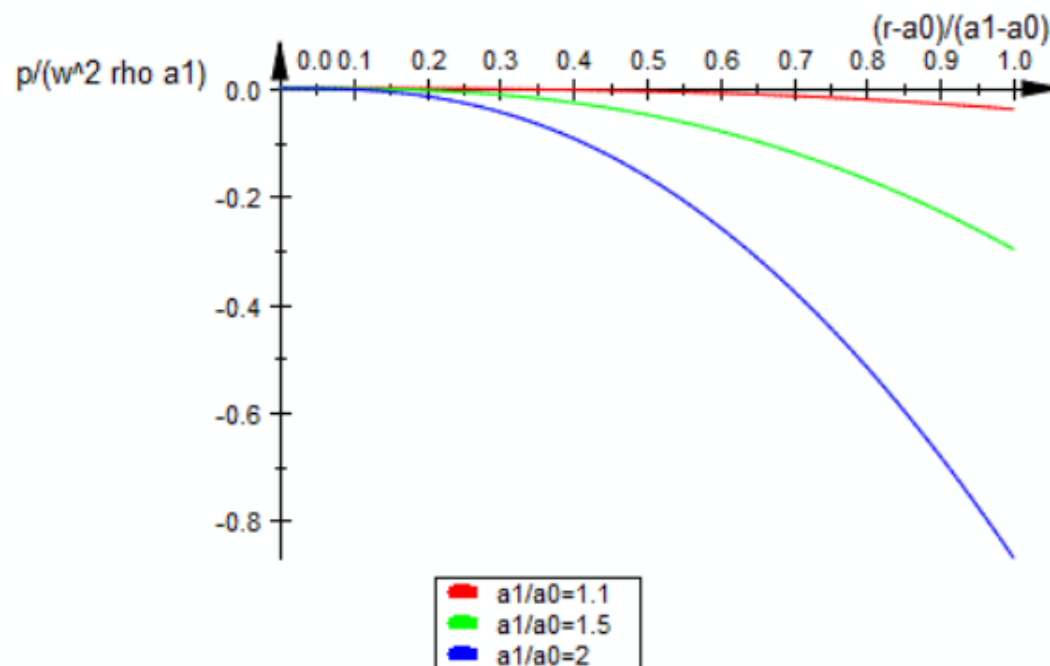
```
plot(
```

```
plot::Function2d(subs(pnorm,a1=1.1),xi=0..1,Color=RGB::Red,Legend="a1/a0=1.1"),
```

```
plot::Function2d(subs(pnorm,a1=1.5),xi=0..1,Color=RGB::Green,Legend="a1/a0=1.5"),
```

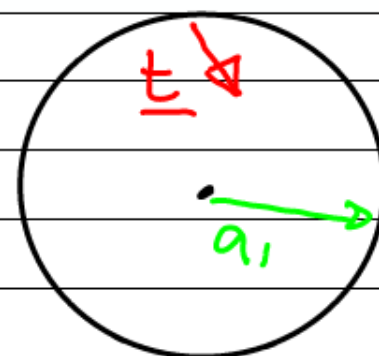
```
plot::Function2d(subs(pnorm,a1=2),xi=0..1,Color=RGB::Blue,Legend="a1/a0=2"),
```

```
AxesTitles = ["(r-a0)/(a1-a0)","p/(w^2 rho a1)"])
```



(f) Find an expression for the torque (per unit out of plane distance) necessary to rotate the external cylinder

Traction exerted on cylinder is equal & opposite to traction acting on fluid



Resultant moment on fluid -

$$\int_0^{2\pi} \underline{r} \times \underline{t} \, a_1 \, d\theta \quad \underline{t} = \underline{n} \cdot \underline{\sigma}$$

$$\underline{\sigma} = \mu \left(\frac{\partial v_\theta}{\partial r} - \frac{v_\theta}{r} \right) (\underline{e}_r \otimes \underline{e}_\theta + \underline{e}_\theta \otimes \underline{e}_r) + p \underline{I}$$

$$\underline{n} = \underline{e}_r$$

$$\underline{t} = p \underline{e}_r + \mu \left(\frac{\partial v_\theta}{\partial r} - \frac{v_\theta}{r} \right) \underline{e}_\theta$$

$$a_1 \underline{e}_r \times \underline{t} = \mu a_1 \left(\frac{\partial v_\theta}{\partial r} - \frac{v_\theta}{r} \right) \underline{e}_z$$

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$$\text{torque} := \text{simplify}(\text{subs}(2*\text{PI}*a1^2*\mu; \text{'*(diff(vqsol,r)-vqsol/r), r=a1}))$$

$$-\frac{4\pi\mu a0^2 a1^2 w}{a0^2 - a1^2} = Q$$

(g) Calculate the rate of external work done by the torque acting on the rotating exterior cylinder

$$W = Q\omega$$

(h) Calculate the rate of internal dissipation in the solid as a function of r .

Dissipation $r_p = \sigma : D$ $\sigma = 2\mu D + pI$

$$= 2\mu D : D + p \underbrace{I : D}_{\text{tr}(D)}$$

$$r_p = 2\mu \left(\frac{\partial v_\theta}{\partial r} - \frac{v_\theta}{r} \right)^2$$

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$$\text{dissip} := \text{simplify}(\mu * (\text{diff}(vqsol, r) - vqsol/r)^2)$$

$$\frac{4\mu a0^4 a1^4 w^2}{r^4 (a0^2 - a1^2)^2}$$

(i) Show that the total internal dissipation is equal to the rate of work done by the external moment.

$$\text{Total dissipation} = \int_{a_0}^{a_1} \tau_p 2\pi r dr$$

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[ assume(a1>a0): assume(a1>0): assume(a0>0):  
  int(dissip*2*PI*r,r=a0..a1)  
  -  $\frac{4 \pi \mu a_0^2 a_1^2 w^2}{a_0^2 - a_1^2}$ 
```

Principle of "Virtual Work"

- "Weak form" of LMB
- Basis for FEA

Let σ be a symmetric tensor on V

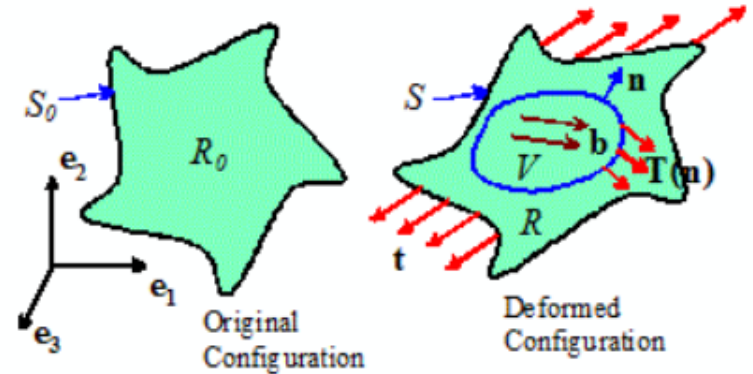
$$\left. \begin{aligned} \sigma \text{ satisfies } \nabla_y \cdot \sigma + \rho \underline{b} &= \rho \frac{\partial \underline{u}}{\partial t} \Big|_x \\ \underline{t} &= \underline{n} \cdot \sigma \end{aligned} \right\} \textcircled{1}$$

Define "Virtual Velocity" field $\delta \underline{u}(\underline{y})$

- arbitrary vector field on V that is

- ① Continuous
- ② Differentiable

$$\text{Let } \delta L = \nabla_y \delta \underline{u} \quad \delta D = \text{sym}(\delta L)$$



Define virtual work as

$$\delta P = \int_V \left(\underline{\sigma} : \underline{\delta D} - \rho \underline{b} \cdot \underline{\delta u} + \rho \left. \frac{\partial u}{\partial t} \right|_{\underline{x}} \cdot \underline{\delta u} \right) dV - \int_S \underline{t} \cdot \underline{\delta u} dA$$

Principle of virtual work

- ① (Not very useful) if $\underline{\sigma}$ satisfies ① then $\delta P = 0$
- ② Useful $\delta P = 0$ for all $\underline{\delta u}$ then $\underline{\sigma}$ satisfies ①

Prove (1) : Start with BLM

$$\int_V \left(\frac{\partial \sigma_{ij}}{\partial y_i} + p b_j - \rho \frac{\partial u_j}{\partial t} \right) \delta u_j dV = 0 \quad (4)$$

Now note $\frac{\partial \sigma_{ij}}{\partial y_i} \delta u_j = \frac{\partial (\sigma_{ij} \delta u_j)}{\partial y_i} - \underbrace{\sigma_{ij}}_{\text{blue}} \frac{\partial \delta u_j}{\partial y_i}$

Note $\int_V \frac{\partial (\sigma_{ij} \delta u_j)}{\partial y_i} dV = \int_S \underbrace{n_i \sigma_{ij} \delta u_j}_{t_j \delta u_j} dA$ $\sigma_{ij} \delta L_{ji} = \sigma_{ij} \delta D_{ij}$

Subst back in (4) :

$$\int_V \left(-\sigma_{ij} \delta D_{ij} + p b_j \delta u_j - \rho \frac{\partial u_j}{\partial t} \delta u_j \right) dV + \int_S t_i \delta u_i dA = 0$$

$$\Rightarrow -\delta p = 0$$

Version (2)

$$\delta P = \int_V \left(\sigma_{ij} \delta D_{ij} - \rho b_j \delta u_j + \rho \frac{\partial u_j}{\partial t} \bigg|_{\underline{x}} \right) dV - \int_S t_j \delta u_j dA = 0 \quad \forall \delta \underline{u}$$

$$\begin{aligned} \text{Note } \sigma_{ij} \delta D_{ij} &= \sigma_{ij} \delta \epsilon_{ji} = \sigma_{ij} \frac{\partial u_j}{\partial y_i} \\ &= \frac{\partial}{\partial y_i} (\sigma_{ij} \delta u_j) - \frac{\partial \sigma_{ij}}{\partial y_i} \delta u_j \end{aligned}$$

Apply div. theorem to first term, collect terms (b)

$$\int_V \left(\frac{\partial \sigma_{ij}}{\partial y_i} - \rho b_j + \rho \frac{\partial u_j}{\partial t} \bigg|_{\underline{x}} \right) \delta u_j dV + \int_S (n_i \sigma_{ij} - t_j) \delta u_j dA = 0 \quad \forall \delta \underline{u}$$
(a)

Choose $\delta u_j = f(y) \left(\frac{\partial \sigma_{ij}}{\partial y_i} - \rho b_j + \rho \frac{\partial u_j}{\partial t} \right)$
 $f(y) = 0$ on S

⑥ = 0 ⑦ integrand is a square - positive or zero everywhere in V

Hence BLM follows (integral can only vanish if integrand = 0)

Similarly let $\delta u_j = t_j - \sigma_{ij} n_i$ on S

$\Rightarrow$ integrand in (b) vanishes

$\Rightarrow \sigma_{ij} n_i = t_j$