

EN 4 HW 6 SOLUTIONS

(1)

1. From last week's MATLAB, we had $M=2\text{ kg}$, $k=25\text{ N/m}$,
 $C=3\text{ N-s/m}$, $x_0=0.1\text{ m}$, and $v_0=-1.0\text{ m/s}$.

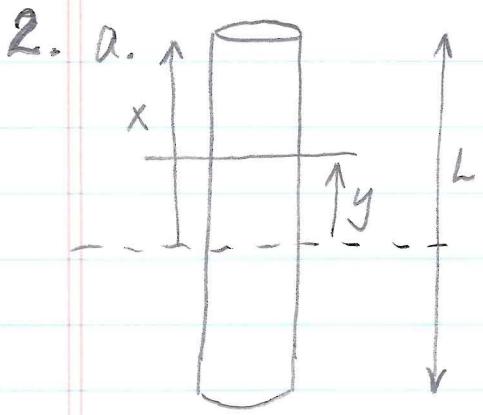
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For a forced vibration, $F(t)=F_0 \sin \omega t$, we need to specify F_0 and examine the steady-state amplitude of vibration X . We normalize X by the static deflection caused by a force F_0 , i.e. $X_0 = F_0/k$.

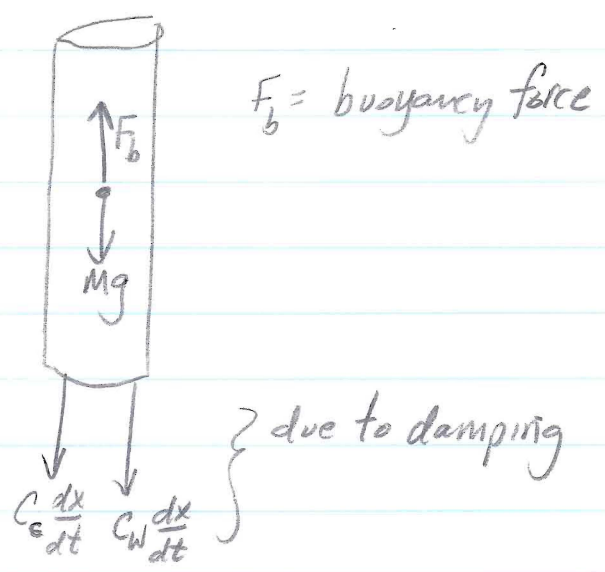
In my MATLAB, I used $F_0 = 1\text{ N}$ so $X_0 = .04\text{ m}$.

For various ω , the response is:

ω (rad/s)	X/X_0	
0.5	~ 1.0	
1.0	~ 1.1	* Natural frequency
1.5	~ 1.2	is $\omega_n = 3.5355$
2.0	~ 1.4	* Damping coeff is
2.5	~ 1.75	$\zeta = 0.2121$
3.0	~ 2.2	* Amplitude at
3.5	~ 2.3	resonance should be
4.0	~ 1.75	$\frac{X}{X_0} \sim \frac{1}{25} = 2.36$
4.5	~ 1.2	
5.0	~ 0.8	
6.0	~ 0.5	
7.0	~ 0.3	



FBD:



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The buoyancy force is

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$$F_b = \underbrace{\rho_w A (L - (x - y))}_{\text{mass of displaced water}} g$$

The force of gravity is

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$$F_g = mg = \rho_b ALg \quad [m = \rho_b AL]$$

b. Summing forces in the vertical direction (positive up),

$$\sum F = F_b - mg - (C_w + C_c) \frac{dx}{dt} = m \frac{d^2x}{dt^2}$$

Using part a,

$$\rho_w A (L - (x - y)) g - \rho_b ALg - (C_w + C_c) \frac{dx}{dt} = \rho_b AL \frac{d^2x}{dt^2}$$

Rearranging,

$$\frac{d^2x}{dt^2} + \frac{C_w + C_c}{\rho_b AL} \frac{dx}{dt} - \frac{\rho_w Ag (L - (x - y))}{\rho_b AL} + g = 0$$

Moving y, which is some y(t), to the right hand side,

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$$\boxed{\frac{d^2x}{dt^2} + \frac{C_w + C_c}{\rho_b AL} \frac{dx}{dt} - \frac{\rho_w g (L - x)}{\rho_b L} - g = \frac{\rho_w g}{\rho_b L} y}$$

+1 c. The static position is obtained by setting $\frac{d^2x}{dt^2} = \frac{dx}{dt} = 0$ and $y=0$ (no motion). Then,

$$-\frac{\rho_w g}{\rho_b L} (L - x_0) - g = 0 \Rightarrow \boxed{x_0 = L \left(1 - \frac{\rho_b}{\rho_w}\right)}$$

+2 d. Let $z = x - x_0$. Then $\frac{d^2z}{dt^2} = \frac{d^2x}{dt^2}$, $\frac{dz}{dt} = \frac{dx}{dt}$, as the constant terms in the E.O.M. drop out:

$$\boxed{\frac{d^2z}{dt^2} + \frac{c_w + c_c}{\rho_b A L} \frac{dz}{dt} + \frac{\rho_w g}{\rho_b L} z = \frac{\rho_w g y}{\rho_b L}}$$

+1 e. $y = y_{\max} \sin \omega t$

f.
$$\frac{d^2z}{dt^2} + \frac{c_w + c_c}{\rho_b A L} \frac{dz}{dt} + \frac{\rho_w g}{\rho_b L} z = \frac{\rho_w g y_{\max}}{\rho_b L} \sin \omega t$$

+2 So, $\boxed{\omega_n = \sqrt{\frac{\rho_w g}{\rho_b L}}}$ (somewhat like a pendulum!)

+1 Then $2\zeta \omega_n = \frac{c_w + c_c}{\rho_b A L} \Rightarrow \zeta = \frac{c_c + c_w}{2\rho_b A L} \sqrt{\frac{\rho_b L}{\rho_w g}} = \boxed{\frac{c_c + c_w}{2A \sqrt{\rho_b \rho_w g L}}}$

+1 and $\frac{F_0}{m} = \frac{\rho_w g y_{\max}}{\rho_b L}$ so $F_0 = \cancel{\rho_b A L} \cdot \frac{\rho_w g y_{\max}}{\cancel{\rho_b L}} = \boxed{\rho_w g A y_{\max}}$

g. $z = \frac{F_0}{m \omega_n^2} M$ in general, where M is the "Magnification factor"

+2 But $\frac{F_0}{m \omega_n^2} = \frac{\rho_w g y_{\max}}{\rho_b L} \left(\frac{\rho_b L}{\rho_w g}\right) = y_{\max}$

so $z = y_{\max} M$ Buoy motion amplified by M over wave motion.

h. For small ζ , we want $\omega_n = \omega$ (Resonance) for a given wave frequency ω . So

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$$\sqrt{\frac{\rho_b g}{\rho_b L}} = \omega \quad \text{or} \quad \boxed{\rho_b L = \frac{\rho_b g}{\omega^2}}$$

Any combo of ρ_b, L (within limits not considered here) that satisfies the above equation will match the buoy response to the wave motion.

+1 i. At resonance, $M \sim \frac{1}{2\zeta}$ so
$$\boxed{Z_{max} = \frac{y_{max}}{2\zeta}}$$

j. Power = (Force) * (Velocity).
The force in the electrical dashpot is $-c_c \dot{z}$. So, the power is

$$P = -c_c \dot{z} \cdot \dot{z} = -c_c \dot{z}^2 \quad (\text{minus indicates energy lost from the buoy motion}).$$

But
$$V = \frac{dz}{dt} = Z_{max} \omega \cos(\omega t + \phi)$$

so
$$\boxed{P = -c_c Z_{max}^2 \omega^2 \cos^2(\omega t + \phi)}$$

Averaging over one period of vibration ($T = \frac{2\pi}{\omega}$) we have

$$\bar{P} = \frac{1}{T} \int_0^T P dt = -c_c Z_{max}^2 \omega^2 \frac{1}{T} \int_0^T \cos^2(\omega t + \phi) dt$$

(Integral: $\frac{\omega}{2\pi} \int_0^{\frac{2\pi}{\omega}} \cos^2(\omega t + \phi) dt = \frac{1}{2}$; do it yourself for practice)

so
$$\bar{P} = \frac{1}{2} c_c Z_{max}^2 \omega^2 = \frac{c_c y_{max}^2 \omega^2}{8\zeta^2} \quad \text{[drop "-" sign now]}$$

j. (cont). Since we are at resonance, $\omega = \omega_n$. And we have ρ from before, so

$$\bar{P} = \frac{c_c y_{\max}^2 4A^2 (\rho_w g^2) \cdot \rho_w g}{8(c_c + c_w)^2 \rho_w g}$$

+1 or

$$\bar{P} = \frac{y_{\max}^2 A^2 \rho_w^2 g^2}{2} \frac{c_c}{(c_c + c_w)^2}$$

k. We now want to maximize \bar{P} with respect to c_c .
So, find c_c where

$$\frac{d\bar{P}}{dc_c} = 0 \Rightarrow \frac{1}{(c_c + c_w)^2} - \frac{2c_c}{(c_c + c_w)^3} = 0$$

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$$\Rightarrow c_c + c_w = 2c_c \Rightarrow \boxed{c_c = c_w}$$

For $c_c = c_w$, $\frac{c_c}{(c_c + c_w)^2} = \frac{1}{4c_w}$

Thus,

$$\boxed{\bar{P} = \frac{y_{\max}^2 A^2 \rho_w^2 g^2}{8c_w}}$$

Check units: Power = $Fv = \text{kg} \cdot \frac{\text{m}}{\text{s}^2} \cdot \frac{\text{m}}{\text{s}} = \text{kg} \cdot \frac{\text{m}^2}{\text{s}^3}$

$$\frac{y_{\max}^2 A^2 \rho_w^2 g^2}{c_w} = \frac{(\text{m}^2)(\text{m}^4)(\text{kg}/\text{m}^3)^2(\text{m}/\text{s}^2)^2}{(\text{kg} \cdot \frac{\text{m}}{\text{s}^2} / \text{m})} = \text{kg} \cdot \frac{\text{m}^2}{\text{s}^3} \quad \checkmark$$

3. This is a "Rotor Excitation" problem.

To solve, we need to know ω_n , J , the mass imbalance Δm , the eccentricity e , and the operating frequency.

Here, we are given

$$\Delta m = 0.5 \text{ kg}, e = 0.3 \text{ m}, J = 0 \text{ (no damping)}$$

$$m = 35 \text{ kg} \text{ and } \omega \Leftrightarrow 275 \text{ RPM}$$

From the static info (35 kg compresses four springs a distance of 0.01 m) we have

$$mg = 4k\delta \quad \delta = 0.01 \text{ m}$$

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so

$$k = \frac{mg}{4\delta} \Rightarrow \omega_n = \sqrt{\frac{4k}{m}} = \sqrt{\frac{g}{\delta}} = 31.32 \frac{\text{rad}}{\text{s}}$$

With 275 RPM corresponding to

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$$\omega = 2\pi \times \frac{275}{60} \text{ rad} = 28.8 \frac{\text{rad}}{\text{s}}$$

the steady-state amplitude of vibration X satisfies

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$$\frac{X}{\left(\frac{\Delta m e}{m}\right)} = \left(\frac{\omega}{\omega_n}\right)^2 M \quad M = \frac{1}{\sqrt{\left(1 - \left(\frac{\omega}{\omega_n}\right)^2\right)^2 + \left(2\frac{\omega}{\omega_n}\right)^2}}$$

Plugging in,

$$X = \frac{\Delta m e}{m} \left(\frac{\omega}{\omega_n}\right)^2 \frac{1}{\left|1 - \left(\frac{\omega}{\omega_n}\right)^2\right|} = \frac{0.5 \text{ kg}}{35 \text{ kg}} 0.3 \text{ m} \left(\frac{28.8}{31.32}\right)^2 \frac{1}{1 - \left(\frac{28.8}{31.32}\right)^2}$$

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$$X = 0.023 \text{ m} = 2.3 \text{ mm}$$

2.3x the static deflection but not too big, perhaps.

4. a. Governing equation is

$$L \frac{dI}{dt} + RI + \frac{1}{C} q = V_0 \sin \omega t$$

Subbing in $I = dq/dt$ yields

$$L \frac{d^2q}{dt^2} + R \frac{dq}{dt} + \frac{1}{C} q = V_0 \sin \omega t$$

+2 or $\boxed{\frac{d^2q}{dt^2} + \frac{R}{L} \frac{dq}{dt} + \frac{1}{LC} q = \frac{V_0}{L} \sin \omega t}$

+1 b. $\omega_n = \sqrt{\frac{1}{LC}}$ (square root of coefficient multiplying q)

c. At steady-state, we have

$$q(t) = Q \sin(\omega t + \phi)$$

where

$$Q = \frac{(V_0/L) M}{\omega_n^2} \text{ since } \frac{F_0}{m} = \frac{V_0}{L} \text{ here}$$

So,

$$I(t) = Q \omega \cos(\omega t + \phi) = I \cos(\omega t + \phi)$$

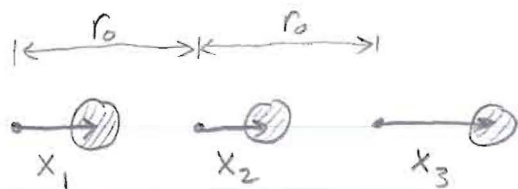
and at $\omega = \omega_n$, $M \approx 1/2\beta$ so

$$I = Q \omega_n M = \frac{V_0/L}{\omega_n^2} \omega_n \cdot \frac{1}{2\beta}$$

From a., $2\beta \omega_n = R/L$ so $\frac{1}{2\beta} = \omega_n L/R$. Hence

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$$I = \frac{V_0/L}{\omega_n} \cdot \omega_n L/R = \boxed{\frac{V_0}{R} = I}$$

5. a.



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b. [assuming equal masses]

$$(1) \quad m \frac{d^2 x_1}{dt^2} = k(x_2 - x_1)$$

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$$(2) \quad m \frac{d^2 x_2}{dt^2} = -k(x_2 - x_1) + k(x_3 - x_2)$$

$$(3) \quad m \frac{d^2 x_3}{dt^2} = -k(x_3 - x_2)$$

c. Let $y = x_2 - x_1$, and $z = x_3 - x_2$.

Now, subtract Eq. 1 from Eq. 2 to get

$$m \frac{d^2 (x_2 - x_1)}{dt^2} = -2k(x_2 - x_1) + k(x_3 - x_2)$$

or

$$\boxed{m \frac{d^2 y}{dt^2} = -2ky + kz}$$

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Subtracting Eq. 2 from Eq. 3 gives

$$m \frac{d^2 (x_3 - x_2)}{dt^2} = -2k(x_3 - x_2) + k(x_2 - x_1)$$

or

$$\boxed{m \frac{d^2 z}{dt^2} = -2kz + ky}$$

d. (1) 3 atoms, 3 directions of motion \Rightarrow 9 degrees of freedom

(2) 3 atoms, 1 direction of motion \Rightarrow 3 degrees of freedom

(3) $3 - 1 = 2$ degrees of freedom for vibrations, matching w/c.

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e. In matrix form,

$$m \frac{d^2}{dt^2} \begin{bmatrix} y \\ z \end{bmatrix} = \begin{bmatrix} -2k & k \\ k & -2k \end{bmatrix} \begin{bmatrix} y \\ z \end{bmatrix}$$

We want the eigenvalues λ^2 of the matrix, which are equal to the natural frequencies squared, ω_n^2 .

We take the determinant:

$$\det \begin{vmatrix} -\frac{2k}{m} - \lambda^2 & \frac{k}{m} \\ \frac{k}{m} & -\frac{2k}{m} - \lambda^2 \end{vmatrix} = \left(-\frac{2k}{m} - \lambda^2\right)^2 - \left(\frac{k}{m}\right)^2 = 0$$

and solve for λ^2 :

$$\lambda^2 = \pm \frac{k}{m} - \frac{2k}{m} = -\frac{k}{m}, -\frac{3k}{m}$$

so the natural frequencies are

$$\omega_n = |\lambda| = \sqrt{\frac{k}{m}}, \sqrt{\frac{3k}{m}}$$

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f. From last week, we already found $\sqrt{\frac{k}{m}} = 6.73 \times 10^{13} \frac{\text{rad}}{\text{s}}$

so

$$\omega_n = 6.73 \times 10^{13} \frac{1}{\text{s}} \text{ and } 11.66 \times 10^{13} \frac{1}{\text{s}}$$

not a spring stiffness.

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The wavenumbers are $k = \frac{\omega_n}{c}$ [see Problem definitions]

and so

$$k = \frac{\omega_n}{3 \times 10^8 \frac{\text{m}}{\text{s}}} = \boxed{1295 \text{ cm}^{-1}, 2243 \text{ cm}^{-1} = k}$$

[Close to actual numbers quoted in HW]

This is in the INFRARED (as discussed in class)

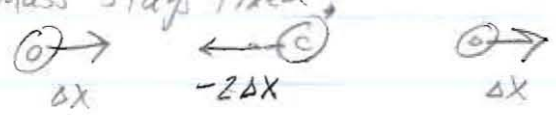
g. If O atoms move oppositely while C is fixed, i.e.



Then the O atoms are like a mass on a spring so

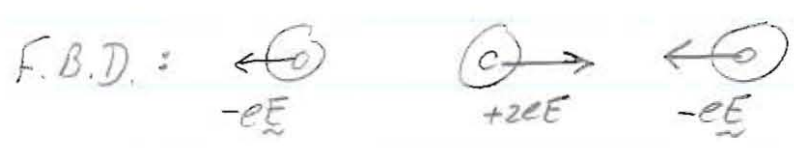
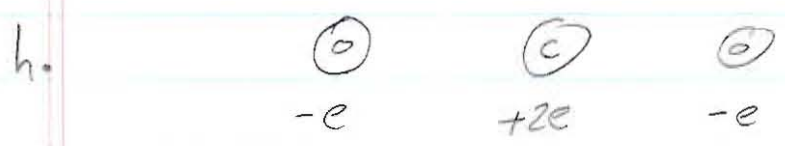
$$\omega_n = \sqrt{\frac{k}{m}} = 6.73 \times 10^{13} \frac{1}{s} \text{ (Wavenumber } 1295 \text{ cm}^{-1}\text{)}$$

If the O atoms move in the same direction while C moves in the other direction, by twice the amount so the center of mass stays fixed;



then the forces on the O atoms are $3k \Delta x$ and one could surmise that the vibration frequency would be $\omega_n = \sqrt{\frac{3k}{m}}$ (Wavenumber 2243 cm^{-1})

These motions can be determined by finding the "eigenvectors" of the eigenvalues λ^2 , as done in class for a slightly different system.



Consistent with the 2243 cm^{-1} mode of vibration

$\omega = \omega_n$ for 2243 cm^{-1} , i.e. $\omega = 11.66 \times 10^{13} \text{ 1/s}$

O_2, N_2 are symmetric. An \underline{E} field cannot force them to vibrate. CH_4 has 2 different atom types and could vibrate (it is worse than CO_2 !!)