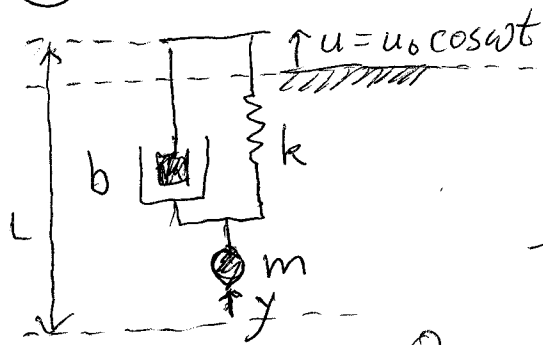


4.12 mistake:  $A(\omega_n) = \frac{u_0 \omega_n^2}{2\beta \omega_n^2} = Q u_0 = (15)(1 \text{ mm}) = \boxed{15 \text{ mm}}$   
on original sdn

4 Better explanation for 4.3



← origin in an inertial frame  
 The acceleration of the mass in the inertial frame is  $\ddot{u} + \ddot{y}$ .

Thus  $-ky - b\dot{y} = m(\ddot{u} + \ddot{y})$

Or  $\boxed{\ddot{y} + 2\beta\omega_n \dot{y} + \omega_n^2 y = -\ddot{u} = \omega^2 u_0 \cos \omega t}$

Mean power input required to maintain the oscillation

is  $\langle P \rangle = \langle (-ky - b\dot{y})\dot{u} \rangle = m \langle \ddot{u}\dot{u} \rangle + m \langle \dot{y}\dot{u} \rangle$

force required to shake top of spring/damper combination  
velocity of top

But  $u = u_0 \cos \omega t$   
 $\Rightarrow \langle \ddot{u}\dot{u} \rangle = u_0 \omega^3 \langle \cos \omega t \sin \omega t \rangle = 0$

so  $\langle P \rangle = m \langle \dot{y}\dot{u} \rangle$ . The steady-state solution to the boxed equation above is  $y = A \cos(\omega t + \phi)$ , with  $\phi$  as in lecture and  $A$  as in lecture with  $\frac{F_0}{m}$  replaced by  $u_0 \omega^2$ .

$A = \frac{u_0 \omega^2}{[(\omega^2 - \omega_n^2)^2 + 4\beta^2 \omega^2 \omega_n^2]^{1/2}}$ . Thus  $\langle P \rangle = m \omega^3 A u_0 \langle \cos(\omega t + \phi) \sin \omega t \rangle$   
 $= -m \omega^3 A u_0 \langle \sin^2 \omega t \rangle \sin \phi$   
 $= -\frac{1}{2} m \omega^3 A \sin \phi$

From lecture,  $\sin \phi = \frac{-2\beta \omega \omega_n}{[(\omega^2 - \omega_n^2)^2 + 4\beta^2 \omega^2 \omega_n^2]^{1/2}}$  ← recall  $Q = \frac{1}{2\beta}$

$\Rightarrow \langle P \rangle = \frac{m}{2} \frac{u_0^2 \omega^5 \cdot 2\beta \omega \omega_n}{(\omega^2 - \omega_n^2)^2 + 4\beta^2 \omega^2 \omega_n^2} = \boxed{\frac{m}{2Q} u_0^2 \omega^4 \frac{\omega_n}{(\omega - \frac{\omega_n^2}{\omega})^2 + \omega_n^2 / Q^2}}$

which is the expression in the original solution