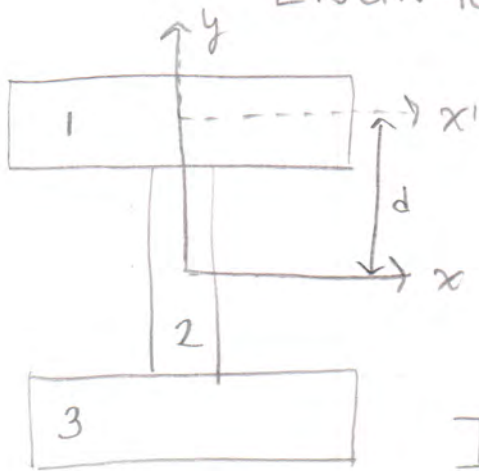


ENGN40 HW6 SOLNS 2016

(a)



$$m = m_1 = m_2 = m_3 = \rho V$$

$$m = 2700(2)(.5)(.5)$$

$$m = 1350 \text{ Kg}$$

$$I_{1x'} = \frac{1}{12} m (.5^2 + .5^2) = 56.25 \text{ Kg}\cdot\text{m}^2$$

parallel axis theorem: $I_{1x} = I_{1x'} + md^2$

$$I_{1x} = 2165 \text{ Kg}\cdot\text{m}^2$$

By symmetry $I_{1x} = I_{3x}$

$$I_{2x} = \frac{1}{12} m (.50^2 + 2^2) = 478 \text{ Kg}\cdot\text{m}^2$$

$$I_x = I_{1x} + I_{2x} + I_{3x} = \boxed{4808 \text{ Kg}\cdot\text{m}^2}$$

b) I_y : no parallel axis theorem needed

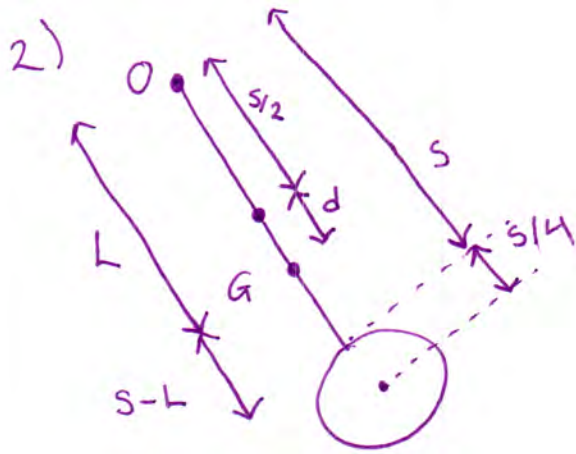
$$I_y = I_{y1} + I_{y2} + I_{y3} = 2I_{y1} + I_{y2}$$

$$I_y = 2 \frac{m}{12} (2^2 + .5^2) + \frac{m}{12} (.5^2 + .5^2) = \boxed{1012.5 \text{ Kg}\cdot\text{m}^2}$$

c) $I_z = I_{z1} + I_{z2} + I_{z3} = I_{z2} + 2I_{z1}$

$$I_z = \frac{1}{12} m (.5^2 + .5^2) + 2 \left[\frac{m}{12} (.5^2 + 2^2) + m (.125^2) \right]$$

$$I_z = \boxed{5231 \text{ Kg}\cdot\text{m}^2}$$



a) center of mass bar
 $= \frac{1}{2} s$
 center of mass disk
 $= \frac{5}{4} s$

$$L = \frac{\frac{1}{2} s m_1 + \frac{5}{4} s m_2}{m_1 + m_2}$$

b)
$$I_{G \text{ bar}} = \frac{1}{12} m_1 s^2 + m_1 d^2$$

$$d = L - s/2$$

$$I_{G \text{ disk}} = \frac{1}{2} m_2 \left(\frac{s}{4}\right)^2 + m_2 (s/4 + s-L)^2$$

$$I_{G \text{ bar}} = m_1 \left(\frac{1}{12} s^2 + (L - s/2)^2 \right) = m_1 \left(\frac{1}{3} s^2 - Ls + L^2 \right)$$

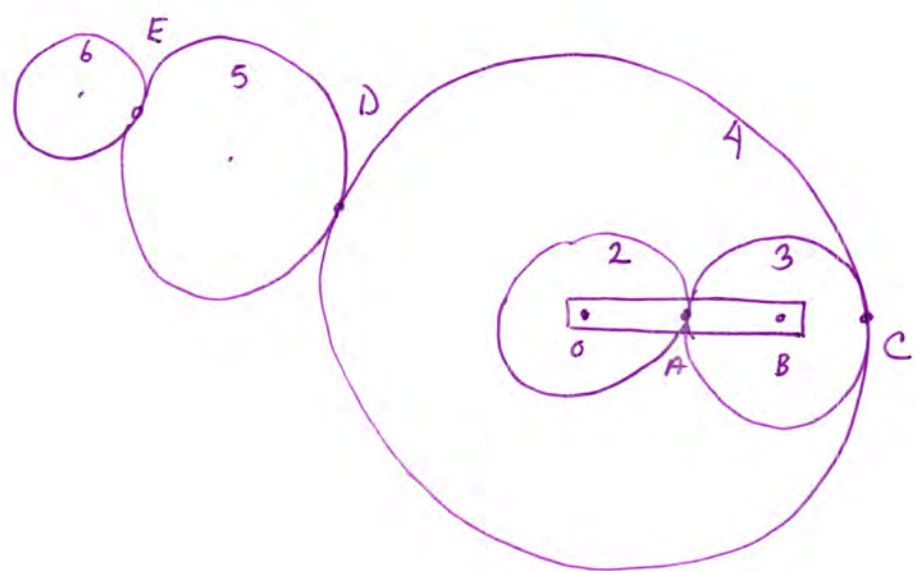
$$I_{G \text{ disk}} = m_2 \left(s^2/32 + (5s/4 - L)^2 \right) = m_2 \left(\frac{5}{32} s^2 - \frac{5}{2} Ls + L^2 \right)$$

$$I_G = I_{G \text{ bar}} + I_{G \text{ disk}}$$

c) From class notes
 $M \rightarrow m_1 + m_2$

$$\omega_n = \sqrt{\frac{L g (m_1 + m_2)}{I_G + L^2 (m_1 + m_2)}}$$

3)



a) $v_E = \omega_6 R_6 = \omega_5 R_5, \omega_5/\omega_6 = R_6/R_5$

$v_D = \omega_5 R_5 = \omega_4 R_4, \omega_4/\omega_5 = R_5/R_4$

$\omega_4/\omega_6 = \omega_4/\omega_5 \cdot \omega_5/\omega_6 = R_5/R_4 \cdot R_6/R_5 = R_6/R_4$

b) Motion of arm: $\underline{v}_B = \underline{\omega}_1 \times \underline{r}_{B/O} = -\omega_1 (R_2 + R_3) \hat{j}$

Motion of gear 3: $\underline{v}_C = \underline{v}_B + \underline{\omega}_3 \times \underline{r}_{C/B} = \underline{v}_B - R_3 \omega_3 \hat{j}$

$\underline{v}_C = \underline{v}_A + \underline{\omega}_3 \times \underline{r}_{C/A} = \underline{v}_A - 2R_3 \omega_3 \hat{j}$

Motion of gear 2: $\underline{v}_A = -\omega_2 R_2 \hat{j}$

eliminate \underline{v}_C : $\underline{v}_B - R_3 \omega_3 \hat{j} = \underline{v}_A - 2R_3 \omega_3 \hat{j}$
 $+ \omega_1 (R_2 + R_3) + R_3 \omega_3 = + \omega_2 R_2 + 2R_3 \omega_3$

$\omega_1 (R_2 + R_3) = \omega_2 R_2 + \omega_3 R_3$

c) E, D, C have zero velocity. gear 4 fixed.

(prior demo with $MG_2 = 0$)

gear 3 $\curvearrowright \omega_3$

$\underline{V}_C = 0$ in equations above

$$0 = -\omega_1 (R_2 + R_3) \hat{j} - R_3 \omega_3 \hat{j}$$

$$0 = -\omega_2 R_2 \hat{j} - 2 R_3 \omega_3 \hat{j}$$

eliminate ω_3

$$0 = 2\omega_1 (R_2 + R_3) - \omega_2 R_2$$

$$\boxed{\frac{\omega_1}{\omega_2} = \frac{2(R_2 + R_3)}{R_2}}$$

d) prior demo $\rightarrow MG_1 = 0, \underline{V}_A = 0$

$$\underline{V}_C = -\omega_4 R_4 \hat{j} = \underline{V}_A + \underline{\omega}_3 \times \underline{r}_{C/A} = -2 R_3 \omega_3 \hat{j}$$

$$-\omega_4 R_4 = -2 R_3 \omega_3$$

The R1 below should be R2

$$\underline{V}_C = -\omega_4 R_4 \hat{j} = \underline{V}_B - R_3 \omega_3 \hat{j} = -\omega_1 (R_1 + R_3) \hat{j} - R_3 \omega_3 \hat{j}$$

eliminate ω_3 : $\frac{\omega_4 R_4}{2} = R_3 \omega_3$

$$+\omega_4 R_4 - \omega_1 (R_1 + R_3) = R_3 \omega_3$$

$$\omega_1 (R_1 + R_3) = \frac{\omega_4 R_4}{2}$$

$$\boxed{\frac{\omega_1}{\omega_4} = \frac{R_4}{2(R_1 + R_3)}}$$

R1 should be R2

Alternative solution to 3(b)

First solve with bar (1)

Stationary

$$\omega_2 R_2 = -\omega_3 R_3$$

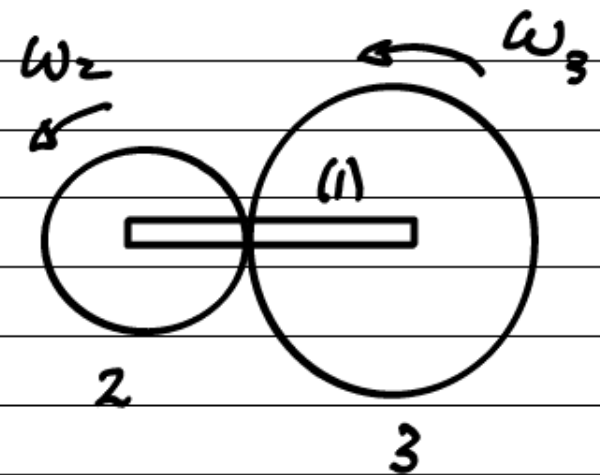
(standard gear formula)

Now note if (1) rotates we can adopt a rotating reference frame that rotates @ same speed as bar (1)

In this frame (2) has angular speed $\omega_2 - \omega_1$, (3) has speed $\omega_3 - \omega_1$ and (1) is stationary

$$\text{Thus } (\omega_2 - \omega_1) R_2 = -(\omega_3 - \omega_1) R_3$$

$$\Rightarrow \omega_2 R_2 + \omega_3 R_3 - \omega_1 (R_2 + R_3) = 0$$



Alternative solution to 3(c), 3(d)

As before adopt a reference frame that rotates with bar (1)

In this frame the angular speeds are 0, $\omega_2 - \omega_1$, $\omega_3 - \omega_1$, $\omega_4 - \omega_1$

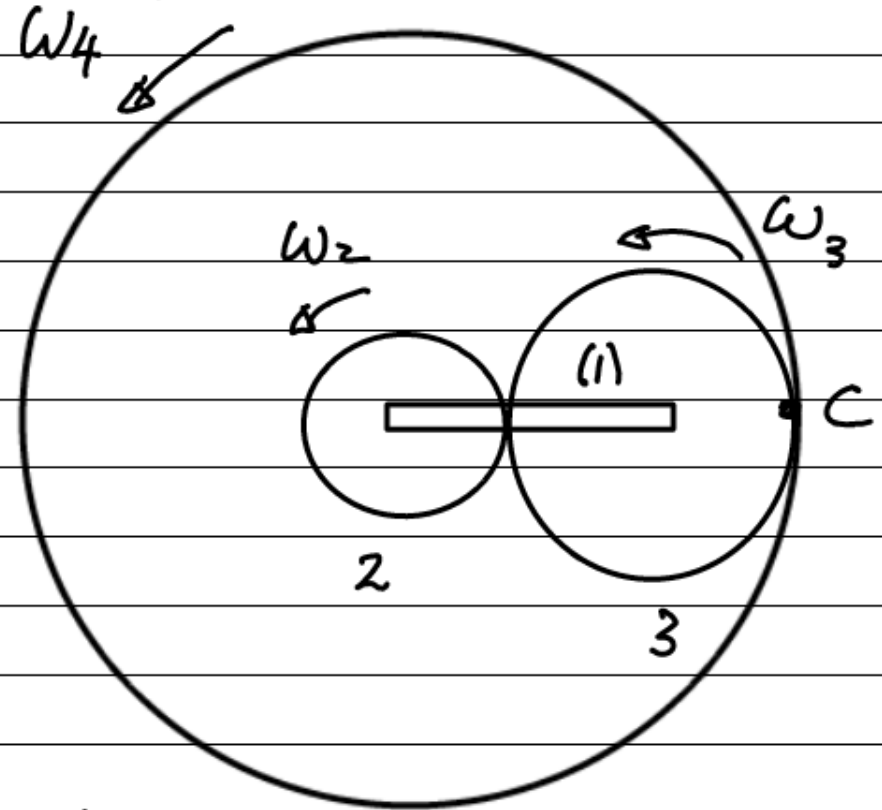
We already know

$$(\omega_2 - \omega_1) R_2 = -(\omega_3 - \omega_1) R_3$$

Since (3)(4) touch @ C $(\omega_3 - \omega_1) R_3 = (\omega_4 - \omega_1) R_4$

Hence $(\omega_2 - \omega_1) R_2 = -(\omega_4 - \omega_1) R_4 = -(\omega_4 - \omega_1) (R_2 + 2R_3)$

For (c) $\omega_4 = 0 \Rightarrow (\omega_2 - \omega_1) R_2 = \omega_1 (R_2 + 2R_3)$



Hence

$$\frac{\omega_2}{\omega_1} = \frac{2(R_2 + R_3)}{R_2} = \frac{R_4 + R_2}{R_2}$$

$$\text{For (d) } \omega_2 = 0 \Rightarrow -\omega_1 R_2 = -(\omega_4 - \omega_1) R_4$$

$$\Rightarrow \frac{\omega_1}{\omega_4} = \frac{R_4}{R_2 + R_4} = \frac{R_4}{2(R_2 + R_3)} = \frac{R_2 + 2R_3}{2(R_2 + R_3)}$$

$$A) \quad \underline{r}_{A/O} = .1 \hat{i} + .25 \hat{j}$$

$$\underline{r}_{B/A} = .5 \hat{i} - .25 \hat{j}$$

$$\underline{v}_A = \underline{\omega}_{OA} \times \underline{r}_{A/O} = -.25 \omega_{OA} \hat{i} + .1 \omega_{OA} \hat{j}$$

$$\underline{v}_B = \underline{v}_A + \underline{\omega}_{AB} \times \underline{r}_{B/A} = -.25 \omega_{OA} \hat{i} + .1 \omega_{OA} \hat{j} + .25 \omega_{AB} \hat{i} + .5 \omega_{AB} \hat{j}$$

constraint on B $\Rightarrow v_{By} = 0$

$$0 = .1 \omega_{OA} \hat{j} + .5 \omega_{AB} \hat{j} \Rightarrow \omega_{OA} = 4 \text{ rad/s}$$

$$\omega_{AB} = -.8 \text{ rad/s}$$

\hat{i} eqn:

$$-.25 \omega_{OA} \hat{i} + .25 \omega_{AB} \hat{i} = -1.2 \text{ m/s}$$

$$\underline{v}_B = -1.2 \text{ m/s } \hat{i}$$

$$\underline{a}_A = \underline{\alpha}_{OA} \times \underline{r}_{A/O} + \underline{\omega}_{OA} \times \underline{\omega}_{OA} \times \underline{r}_{A/O} = -.25 \alpha_{OA} \hat{i} + .1 \alpha_{OA} \hat{j} - .1 \omega_{OA}^2 \hat{i} - .25 \omega_{OA}^2 \hat{j}$$

$$\underline{a}_A = -2.1 \hat{i} - 3.8 \hat{j}$$

$$\underline{a}_B = \underline{a}_A + \underline{\alpha}_{AB} \times \underline{r}_{B/A} + \underline{\omega}_{AB} \times \underline{\omega}_{AB} \times \underline{r}_{B/A}$$

$$\underline{a}_B = \underline{a}_A + .25 \alpha_{AB} \hat{i} + .5 \alpha_{AB} \hat{j} - .5 \omega_{AB}^2 \hat{i} + .25 \omega_{AB}^2 \hat{j}$$

$$\hat{j}: \quad 0 = -3.8 + .5 \alpha_{AB} + .25 (-.8)^2 \Rightarrow \alpha_{AB} = +7.28 \text{ rad/s}^2$$

$$\hat{i}: \quad a_{Bx} = -2.1 + .25 \alpha_{AB} - .5 \omega_{AB}^2 \Rightarrow a_{Bx} = -0.6 \text{ m/s}^2$$

5. $\omega = \text{constant}$ $\Theta = \int \omega dt = \underbrace{\theta_0}_0 + \omega t$, $\Theta = \omega t$

a) $\underline{v}_B = \underline{\omega} \times \underline{r}_{B/A}$, $\underline{r}_{B/A} = R \sin \theta \hat{i} - R \cos \theta \hat{j}$

$$\underline{v}_B = R \cos(\omega t) \cdot \omega \hat{i} + R \sin(\omega t) \cdot \omega \hat{j}$$

b) $\underline{v}_C = \underline{v}_B + \underline{\omega}_{BC} \times \underline{r}_{C/B}$, $\underline{r}_{C/B} = -L_1 \sin \beta \hat{i} - L_1 \cos \beta \hat{j}$

$$\underline{v}_C = \underline{v}_B + \omega_{BC} L_1 \cos \beta \hat{i} - \omega_{BC} L_1 \sin \beta \hat{j}$$

$$\underline{v}_C = (R\omega \cdot \cos \omega t + \omega_{BC} L_1 \cos \beta) \hat{i} + (R\omega \cdot \sin(\omega t) - \omega_{BC} L_1 \sin \beta) \hat{j}$$

c) $\underline{v}_C = \underline{v}_D + \underline{\omega}_{CD} \times \underline{r}_{C/D}$, $\underline{r}_{C/D} = -L_2 \cos \phi \hat{i} - L_2 \sin \phi \hat{j}$

$$\underline{v}_C = \omega_{CD} L_2 \sin \phi \hat{i} - \omega_{CD} L_2 \cos \phi \hat{j}$$

d) set b) & c) equal

$$\hat{i}) R\omega \cdot \cos \omega t + \omega_{BC} L_1 \cos \beta = \omega_{CD} L_2 \sin \phi$$

$$\hat{j}) R\omega \sin \omega t - \omega_{BC} L_1 \sin \beta = -\omega_{CD} L_2 \cos \phi$$

R, ω, L_1, L_2 known

$\omega_{BC}, \omega_{CD}, \beta, \phi$ unknown

e) Geometry: $\underline{r}_{C/A} + \underline{r}_{D/C} = \underline{r}_{D/A} = \underbrace{D_x \hat{i} - D_y \hat{j}}_{\text{fixed distance}} = \text{constant}$

$$\underline{r}_{C/A} = \underline{r}_{C/B} + \underline{r}_{B/A}$$

$$D_x \hat{i} - D_y \hat{j} = \underline{r}_{C/B} + \underline{r}_{B/A} + \underline{r}_{D/C}$$

$$\hat{i}) D_x = -L_1 \sin \beta + R \sin \omega t + L_2 \cos \phi$$

$$\hat{j}) -D_y = -L_1 \cos \beta - R \cos \omega t + L_2 \sin \phi$$