

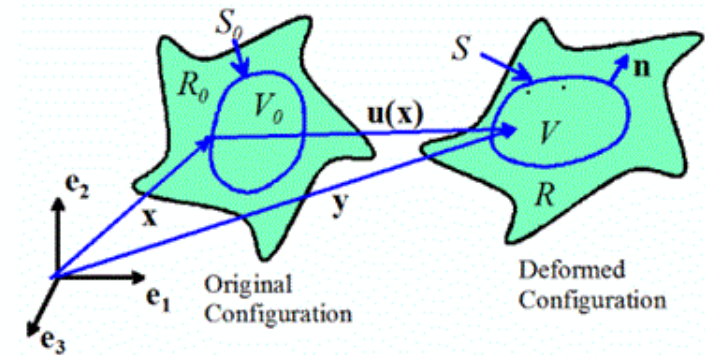
Review

Transport Relations

V Material vol in current config

V_0 Material vol in ref config

$\phi(\mathbf{x})$ Any scalar material property



$$\frac{d}{dt} \int_V \phi dV = \int_V \left(\frac{\partial \phi}{\partial t} \Big|_{\mathbf{x}} + \phi L_{kk} \right) dV = \int_V \left(\frac{\partial \phi}{\partial t} \Big|_{\mathbf{y}} + \nabla_{\mathbf{y}} \cdot (\phi \mathbf{v}) \right) dV = \int_V \frac{\partial \phi}{\partial t} \Big|_{\mathbf{y}} dV + \int_S \phi \mathbf{v} \cdot \mathbf{n} dA$$

Proof \rightarrow $\frac{d}{dt} \int_V \phi dV = \frac{d}{dt} \int_{V_0} \phi J dV_0 = \int_{V_0} \left(\frac{\partial \phi}{\partial t} \Big|_{\mathbf{x}} + \phi \frac{dJ}{dt} \right) dV_0$

Recall $\frac{dJ}{dt} = J \operatorname{tr}(L) = J \operatorname{tr}(D)$ \square

$$\Rightarrow * = \int_{V_0} \left(\frac{\partial \phi}{\partial t} \Big|_{\mathbf{x}} + \phi \operatorname{tr}(L) \right) J dV_0 = \int_V \left(\frac{\partial \phi}{\partial t} \Big|_{\mathbf{y}} + \phi \operatorname{tr}(L) \right) dV$$

Now recall $\frac{\partial \phi}{\partial t} \Big|_{\underline{y}} = \frac{\partial \phi}{\partial t} \Big|_{\underline{y}} + \underbrace{\nabla_{\underline{y}} \phi}_{\text{tr}(\underline{L})} \cdot \underline{v}$

$\Rightarrow \square = \frac{\partial \phi}{\partial t} \Big|_{\underline{y}} + \underbrace{(\nabla_{\underline{y}} \phi) \cdot \underline{v} + \phi \nabla_{\underline{y}} \cdot \underline{v}}_{\nabla \cdot (\phi \underline{v})}$

$L_{ii} = \frac{dv_i}{dy_i} = \nabla_{\underline{y}} \cdot \underline{v}$

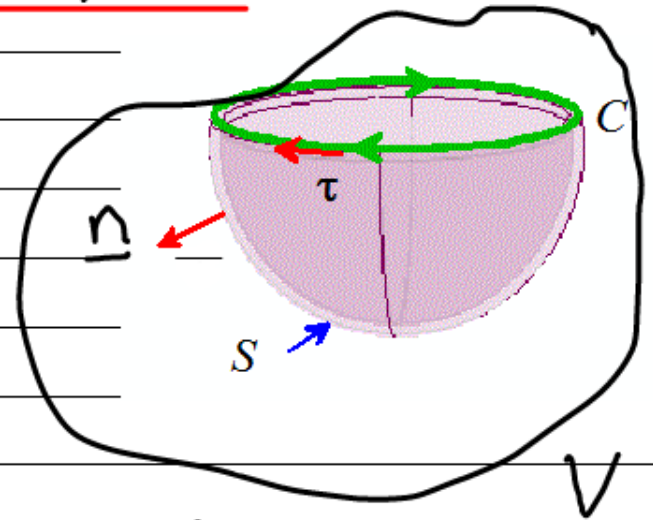
Finally note $\int_V \nabla_{\underline{y}} \cdot (\phi \underline{v}) dV = \int_S \underline{n} \cdot (\phi \underline{v}) dA$
(Divergence theorem)

Transport Relations for curves and surfaces

Define C : curve in current config
 C_0 : curve in ref config

$\underline{\tau}$: Tangent to curve

S : surface in deformed solid
 \underline{n} : normal



$$1. \quad \frac{d}{dt} \int_C \phi \tau_i ds = \int_C \left(\delta_{ij} \frac{\partial \phi}{\partial t} \Big|_{\mathbf{x}=\text{const}} + \phi \frac{\partial v_i}{\partial y_j} \right) \tau_j ds$$

$$2. \quad \frac{d}{dt} \int_S \phi n_i dA = \int_S \left(\delta_{ij} \frac{\partial \phi}{\partial t} \Big|_{\mathbf{x}=\text{const}} + \delta_{ij} \phi \frac{\partial v_k}{\partial y_k} - \phi \frac{\partial v_j}{\partial y_i} \right) n_j dA$$

$$\underbrace{(\underline{\tau} ds)}_{\text{material fiber in curr config}} = \underbrace{F \underline{v}_0 ds_0}_{\text{Ref config}}$$

$$\text{Proof: } \frac{d}{dt} \int_C \varphi \underline{\tau} ds = \frac{d}{dt} \int_{C_0} \varphi F \underline{\tau}_0 ds_0$$

$$\therefore = \int_{C_0} \left(\frac{\partial \varphi}{\partial t} \Big|_x \underline{F} + \varphi \frac{\partial F}{\partial t} \underbrace{F^{-1} F}_{\mathbf{I}} \right) \underline{\tau}_0 ds_0$$

$$= \int_{C_0} \left(\frac{\partial \varphi}{\partial t} \Big|_x + \varphi \nabla_g \underline{V} \right) F \underline{\tau}_0 ds_0$$

$$= \int_C \left(\frac{\partial \varphi}{\partial t} \Big|_x + \varphi \nabla_g \underline{V} \right) \underline{\tau} ds$$

After completing ENGN2210 you should

Be familiar with linear vector spaces relevant to continuum mechanics and able to perform vector and tensor manipulations in Cartesian and curvilinear coordinate systems

Be able to describe motion, deformation and **forces** in a continuum;

Be able to derive equations of motion and conservation laws for a continuum ;

Understand constitutive models for fluids and viscoelastic solids;

Be able to solve simple boundary value problems for fluids and solids.

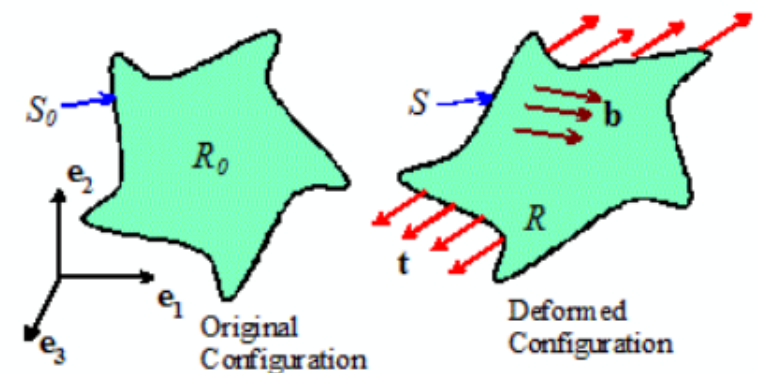
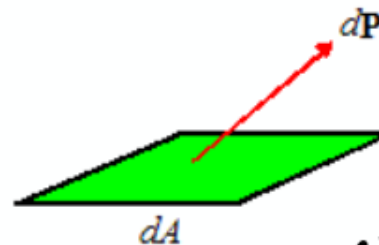
Up next!

4 Kinetics : Description of internal forces in continua

External Forces

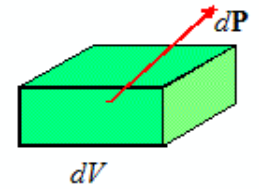
External Traction

$$\underline{t} = \lim_{dA \rightarrow 0} \frac{dP}{dA}$$



All defined on deformed config

Body force (per unit mass)



$$\underline{b} = \lim_{dV \rightarrow 0} \frac{d\underline{P}}{\rho dV}$$

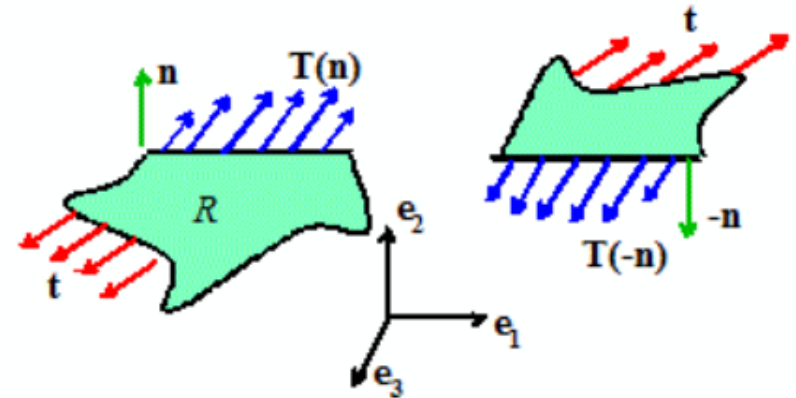
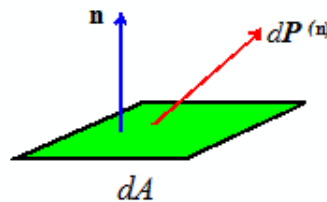
ρ : mass per unit deformed vol

Resultant force $\underline{P} = \int_S \underline{t} dA + \int_V \rho \underline{b} dV$

Internal Forces

Internal Traction Vector

$$\underline{T}(\underline{n}) = \lim_{dA \rightarrow 0} \frac{d\underline{P}(\underline{n})}{dA}$$



Internal traction depends on orientation \underline{n}

Cauchy Stress Tensor

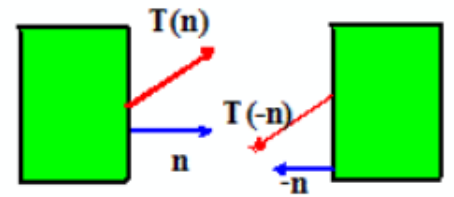
Define stress tensor σ satisfying

$$\underline{T}(\underline{n}) = \underline{n} \sigma$$

(note: some authors say $\sigma \underline{n} = \underline{T}(\underline{n})$)

Existence of σ is a consequence of Newton's Laws

① Newton I $\underline{T}(-\underline{n}) = -\underline{T}(\underline{n})$



② Newton III $\underline{F} = m\underline{a}$ for "Cauchy Tetrahedron"

$$\underline{T}(\underline{n}) dA_n + \sum_{i=1}^3 \underline{T}(-\underline{e}_i) dA_i + \rho \underline{b} dV$$

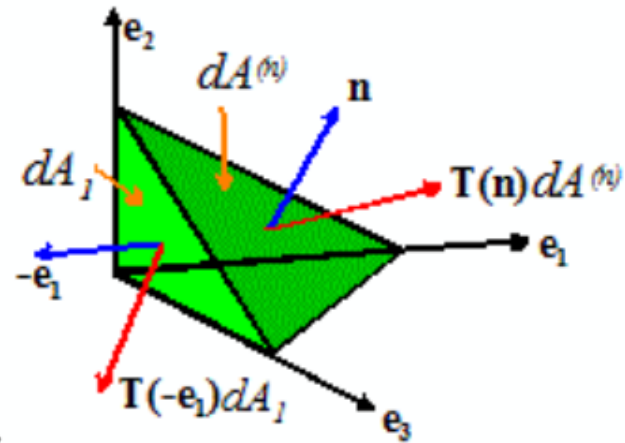
$$= \rho dV \underline{a}$$

Note that $\lim_{dV \rightarrow 0} \frac{dA_i}{dA_n} = n_i$ (see Appendix E of solidmechanics.org)

$$\lim_{dV \rightarrow 0} \frac{dV}{dA_n} = 0$$

$$\Rightarrow \underline{T}(\underline{n}) - \sum_{i=1}^3 \underline{T}(\underline{e}_i) n_i = 0$$

$$\text{Define } T_j(\underline{e}_i) = \sigma_{ij}$$



$$T_j(\underline{n}) = n_i \sigma_{ij}$$

Maps a vector onto a vector $\Rightarrow \sigma_{ij}$ is a tensor