

# Review

Solving acoustics problems:

Wave speed  $c_s = \sqrt{\left. \frac{\partial p}{\partial \rho} \right|_{s=\text{const}}} = \sqrt{\gamma R \theta_0}$

Flow potential  $\frac{\partial^2 \Omega}{\partial t^2} = c_s^2 \frac{\partial^2 \Omega}{\partial y_i \partial y_i}$

Boundary conditions:  $\frac{\partial \Omega}{\partial y_i} n_i = V_n^*$  (surfaces with known velocity)

$-\rho_0 \frac{\partial \Omega}{\partial t} = p^*$  (boundaries with known pressure)

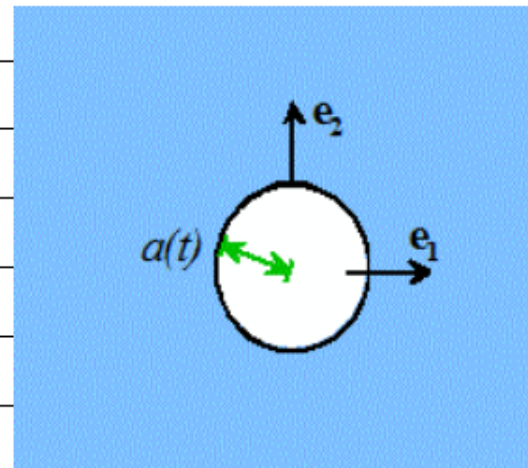
Velocity:  $v_i = \frac{\partial \Omega}{\partial y_i}$       Pressure:  $p = -\rho_0 \frac{\partial \Omega}{\partial t}$

Example: Vibrating sphere

$$a(t) = a_0 + A e^{i\omega t} \quad A \ll a_0$$

Try a potential of form  $\Omega = \frac{1}{r} f(t - r/c_s)$

Substitute into wave eq: straightforward  
to show  $\frac{\partial^2 \Omega}{\partial t^2} = c_s^2 \nabla_y^2 \Omega$



$$n_i = y_i / a_0$$

Boundary conditions

$$i\omega A e^{i\omega t} = v_i n_i = - \int \frac{f(t - a_0/c_s)}{a_0^2} + \frac{1}{a_0 c_s} f'(t - a_0/c_s) \left] \frac{y_i}{A} \frac{y_i}{a_0} \right. = 1$$

Assume  $f(t) = C e^{i\omega t}$

$$-i\omega a_0^2 A e^{i\omega t} = C e^{i\omega t - i\omega a_0/c_s} \left[ 1 + \frac{i\omega a_0}{c_s} \right]$$

$$\Rightarrow C = \frac{-i\omega a_0^2 A e^{i\omega a_0/c_s}}{\left[1 + \frac{i\omega a_0}{c_s}\right]}$$

$$\text{Now } u_i = \frac{\partial \Omega}{\partial y_i} = -C e^{i\omega(t - r/c_s)} \left[ \frac{1}{r^2} + \frac{i\omega}{rc_s} \right] \frac{y_i}{r}$$

$$p = -\rho_0 \frac{\partial \Omega}{\partial t} =$$

$$\text{Far field behavior } u_i = \frac{1}{r} f'(t - r/c_s) \frac{y_i}{r}$$

- "monopole"

Can generate more solutions by taking spatial derivatives of this function

$$\text{eg } \frac{\partial u_i}{\partial y_j} \text{ - "dipole"}$$

## 7) Elasticity

\* Goal: understand large strain elasticity  
- Linearize  $\Rightarrow$  linear elasticity

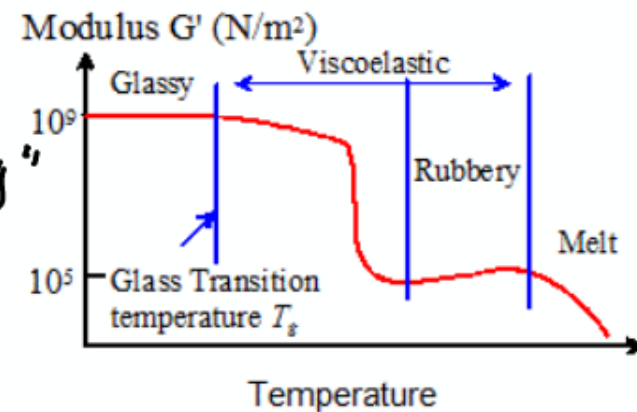
\* Material models for elastic materials

(1) Linear elasticity - models reversible deformation in most solid materials @ low stresses

(2) hyperelastic - model polymers experiencing large strains in "rubbery" regime

\* General behavior of cross-linked polymer:

- ⊙ low temp stiff/brittle "glassy"
- ⊙ intermediate - softens; rate & history dependent
- ⊙ high temp: "rubbery"



## \* Features of rubbery regime

- (1) Low shear modulus ( $\sim 2 \text{ GPa}$ )
  - (2) High bulk modulus ( $\sim 100 \text{ GPa}$ )
  - (3) Modulus increases with temp
  - (4) Gives off heat when stretched
  - (5) History independent  
Rate independent  
Reversible
- } approximately

Hyperelastic material models approximate this regime of behavior

## Structure of hyperelastic material models

Assume: Local action

: No history dependence : state is completely specified by  $F$ ;  $\theta$

We will show that constitutive equations have the following structure

Specific internal energy	$\varepsilon = \hat{\varepsilon}(C, \theta)$	$C = F^T F$
" entropy	$s = \hat{s}(C, \theta)$	
Helmholtz	$\psi = \hat{\psi}(C, \theta)$	

Stress response function  $\underline{\Sigma} = \hat{\underline{\Sigma}}(C, \theta)$

Heat transfer response funct  $\underline{Q} = \hat{\underline{Q}}(C, \theta, \nabla \theta)$