

Review: Field equations of linear elasticity

Strain-displacement relation:
$$\varepsilon_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

Constitutive equation:
$$\sigma_{ij} = C_{ijkl} (\varepsilon_{kl} - \alpha_{kl} \Delta \theta)$$

Isotropic material:
$$C_{ijkl} = \mu (\delta_{il} \delta_{jk} + \delta_{ik} \delta_{jl}) + \lambda \delta_{ij} \delta_{kl}$$

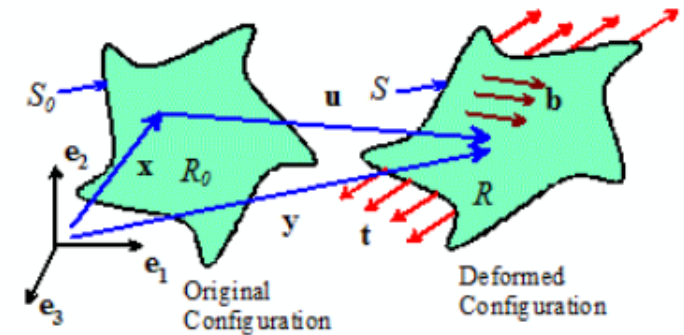
$$\nu = \frac{\lambda}{2(\mu + \lambda)} \quad E = 2\mu(1 + \nu)$$

$$\varepsilon_{ij} = \frac{1 + \nu}{E} \sigma_{ij} - \frac{\nu}{E} \sigma_{kk} \delta_{ij} + \alpha \Delta \theta \delta_{ij}$$

$$\sigma_{ij} = \frac{E}{1 + \nu} \left\{ \varepsilon_{ij} + \frac{\nu}{1 - 2\nu} \varepsilon_{kk} \delta_{ij} \right\} - \frac{E \alpha \Delta \theta}{1 - 2\nu} \delta_{ij}$$

Linear Momentum:
$$\frac{\partial \sigma_{ij}}{\partial x_i} + \rho b_j = \rho \frac{\partial^2 u_j}{\partial t^2}$$

Boundary Conditions:
$$u_i = u_i^*(t) \quad \text{on } S_1 \quad \sigma_{ij} n_i = t_j^*(t) \quad \text{on } S_2$$



Simplifying Governing Equations

LMB in terms of \underline{u} : Cauchy-Navier equation

Eliminate σ , ε ; Note also $C_{ijkl} \varepsilon_{kl} = C_{ijkl} \frac{1}{2} \left(\frac{\partial u_k}{\partial x_l} + \frac{\partial u_l}{\partial x_k} \right)$

But $C_{ijkl} = C_{ijlk} \Rightarrow C_{ijkl} \varepsilon_{kl} = C_{ijne} \frac{\partial u_n}{\partial x_e}$

Hence
$$\frac{\partial}{\partial x_j} \left\{ C_{ijkl} \frac{\partial u_k}{\partial x_e} \right\} + \rho b_i = \rho \frac{\partial^2 u_i}{\partial t^2}$$

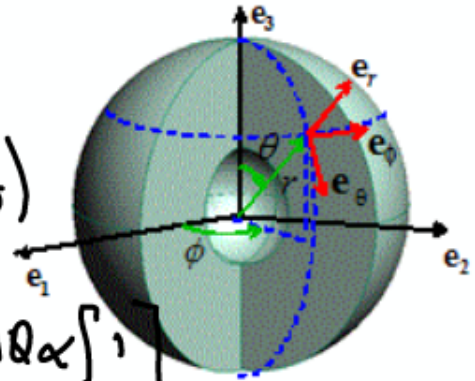
For isotropic homogeneous material; no temp change

$$\frac{1}{1-2\nu} \frac{\partial^2 u_j}{\partial x_j \partial x_i} + \frac{\partial^2 u_i}{\partial x_j \partial x_j} + \rho b_i = \rho \frac{\partial^2 u_i}{\partial t^2}$$

$$\frac{1}{1-2\nu} \nabla \nabla \cdot \underline{u} + \nabla^2 \underline{u} + \rho \underline{b} = \rho \frac{\partial^2 \underline{u}}{\partial t^2}$$

Example: Spherical symmetry

Strain-displacement $\underline{\varepsilon} = \frac{\partial u}{\partial r} \underline{e}_r \otimes \underline{e}_r + \frac{u}{r} (\underline{e}_\theta \otimes \underline{e}_\theta + \underline{e}_\phi \otimes \underline{e}_\phi)$



Stress-strain law

$$\begin{bmatrix} \sigma_{rr} \\ \sigma_{\theta\theta} \end{bmatrix} = \frac{2\mu}{1-2\nu} \begin{bmatrix} 1-\nu & 2\nu \\ \nu & 1 \end{bmatrix} \begin{bmatrix} \frac{\partial u}{\partial r} \\ \frac{u}{r} \end{bmatrix} \sim \frac{2\mu(1+\nu)\Delta\theta\alpha}{1-2\nu} \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

Euler-Lagrange (ELB): $\frac{\partial \sigma_{rr}}{\partial r} + \frac{2}{r} (\sigma_{rr} - \sigma_{\theta\theta}) + \rho b_r = \rho \frac{\partial^2 u}{\partial t^2}$

Combine: $\frac{d}{dr} \left(\frac{1}{r^2} \frac{\partial}{\partial r} (r^2 u_r) \right) = \frac{\alpha(1+\nu)}{1-\nu} \frac{\partial \Delta\theta}{\partial r} + \frac{1-2\nu}{2\mu(1-\nu)} \left[\frac{\partial^2 u}{\partial t^2} - \rho b_r \right]$

Boundary conditions: $\left. \begin{array}{l} \text{prescribe } u_r \\ \text{or } \sigma_{rr} \end{array} \right\} \begin{array}{l} r=a \\ r=b \end{array}$

A solid, spherical nuclear fuel pellet with outer radius a is subjected to a uniform internal distribution of heat due to a nuclear reaction. The heating induces a steady-state temperature field

$$\theta(r) = \Delta\theta \frac{r^2}{a^2} + \theta_0$$

Calculate the distribution of stress in the pellet.



Procedure: (1) Solve ODE for $u(r)$ using $u(0) = 0$
- 1 arbitrary constant

(2) Solve for constant using $\sigma_{rr} = 0$ @ $r = a$

Solution:
$$\sigma_{rr} = \frac{4\alpha \Delta\theta \mu (a^2 - r^2) (1 + \nu)}{5a^2(1 - \nu)}$$

$$\sigma_{\theta\theta} = \frac{4\alpha \Delta\theta \mu (a^2 - 2r^2)}{5a^2(1 - \nu)}$$

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[ assume(-1<`&nu;`<1/2);
[ assume(EE>0);
[ assume(a>0);
[ assume(r>0);
[ T := DT*r^2/a^2+T0;
[ ode1 := diff(diff(r^2*uu(r),r)/r^2,r) = `&alpha;`*(1+`&nu;`)/(1-`&nu;`)*diff(T,r);

$$\frac{2uu(r)+r^2\frac{\partial^2}{\partial r^2}uu(r)+4r\frac{\partial}{\partial r}uu(r)}{r^2} - \frac{2(2ru(r)+r^2\frac{\partial}{\partial r}uu(r))}{r^3} = -\frac{2\alpha DT r(v+1)}{a^2(v-1)}$$

[ u := simplify(solve(ode({ode1,uu(0)=0},uu(r))))[1]

$$-\frac{r(5vC8a^2-5C8a^2+3\alpha DT r^2+3\alpha vDT r^2)}{15a^2(v-1)}$$

[ srr := eval(EE/(1+`&nu;`)/(1-2*`&nu;`
* ((1-`&nu;`)*diff(u,r) + 2*`&nu;`*u/r) - EE*`&alpha;`*T/(1-2*`&nu;`)):
[ C8val := solve(subs(srr,r=a),C8):
[ srrfull := simplify(subs(srr,C8=C8val))

$$\left\{ -\frac{2\alpha DTEE(a^2-r^2)}{5a^2(v-1)} \right\}$$

[ sqq := eval(EE/(1+`&nu;`)/(1-2*`&nu;`
* (`&nu;`*diff(u,r) + u/r) - EE*`&alpha;`*T/(1-2*`&nu;`)):
[ sqqfull := simplify(subs(sqq,C8=C8val))

$$\left\{ -\frac{2\alpha DTEE(a^2-2r^2)}{5a^2(v-1)} \right\}$$


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Potential Solutions for 3D static linear elasticity

Goal : Simplify Navier equation

Assumptions : Constant temperature
Isotropic
Homogeneous

Define Papkovitch-Neuber potentials $\underline{\psi}$, ϕ
satisfying

$$\nabla^2 \underline{\psi} = -\rho \underline{b} \quad \nabla^2 \phi = -\underline{x} \cdot \underline{b}$$

Then define : $\underline{u} = \frac{1}{\mu} \left(\underline{\psi} + \frac{1}{4(1-\nu)} \nabla(\phi - \underline{x} \cdot \underline{\psi}) \right)$

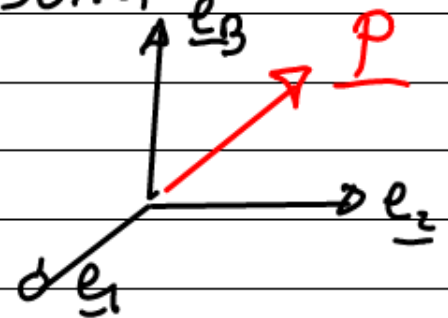
Then C-N equation satisfied automatically
(This representation is complete)

Also useful:

$$2(1-\nu)\sigma_{ij} = 2\nu \frac{\partial \psi_k}{\partial x_k} \delta_{ij} + (1-2\nu) \left(\frac{\partial \psi_i}{\partial x_j} + \frac{\partial \psi_j}{\partial x_i} \right) + x_k \frac{\partial^2 \psi_k}{\partial x_i \partial x_j} + \frac{\partial^2 \psi}{\partial x_i \partial x_j}$$

Example: Point force in an infinite solid (acting at origin)

Point force is a Dirac Delta distribution of body force



$$\underline{\rho b}(\underline{x}) = \underline{P} \delta(\underline{x})$$

$\delta(\underline{x})$ is a delta distribution with property

$$\int_V \delta(\underline{x}) f(\underline{x}) dV = f(\underline{0})$$

Hence we seek $\underline{\psi}$, ϕ satisfying

$$\nabla^2 \underline{\psi} = -\delta(\underline{x}) \underline{P} \quad \nabla^2 \phi = 0$$

Guess $\underline{\psi} = G(r) \underline{P} \quad \phi = 0$

Substitute and integrate over sphere radius r surrounding origin

$$\underline{P} \int_V \nabla \cdot \nabla G(r) dV = -\underline{P} \int_V \delta(\underline{x}) dV = -\underline{P}$$

Div theorem $\underline{P} \int_A \nabla G(r) \cdot \underline{n} dA = -\underline{P}$

$$4\pi r^2 \frac{dG}{dr} = -1 \quad \Rightarrow \quad G = \frac{1}{4\pi r} \quad r = \sqrt{x_k x_k}$$

$$\text{Hence } \underline{\psi} = \frac{P}{4\pi r} \quad \emptyset = 0$$

$$\text{Hence } u_i = \frac{1}{16\pi(1-\nu)r} \left\{ \frac{P_k x_k x_i}{r^2} + (3-4\nu) P_i \right\}$$

$$\sigma_{ij} = \frac{-1}{8\pi(1-\nu)r} \left\{ \frac{3P_k x_k x_i x_j}{r^3} + \frac{(1-2\nu)}{r} (P_i x_j + P_j x_i - P_k x_k \delta_{ij}) \right\}$$