

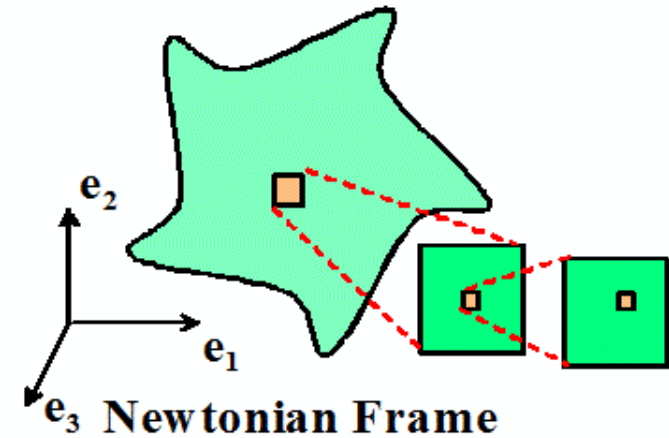
Review: Kinematics of Continua

Assumptions:

1. Existence of a Newtonian Frame

Idealized as \mathbb{R}^3
Inertial basis $\{\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3\}$

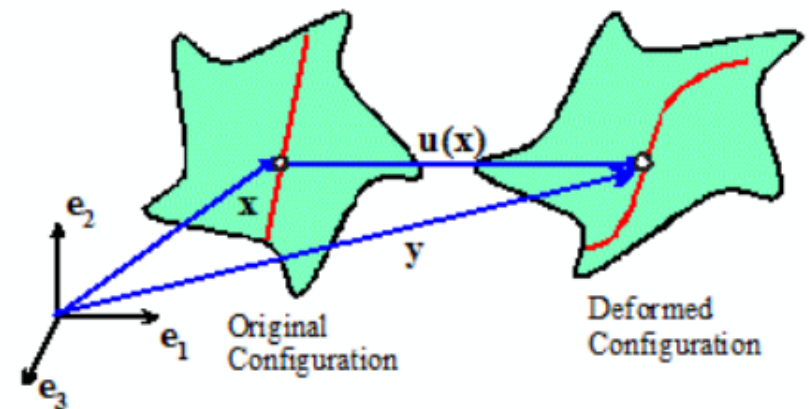
2. Matter is infinitely divisible, and locally homogeneous



3.2 Describing Deformation

"Configuration": Region of \mathbb{R}^3 occupied by solid or fluid

"Reference" config: Any convenient fixed configuration - e.g. initial config



Current config: region occupied @ time t

\underline{x} : Position in reference config

\underline{y} : Position in current config

Deformation Mapping $\underline{y}(\underline{x}, t)$: specifies position after deformation

\underline{y} is continuous & differentiable
 $\det \left(\frac{\partial y_i}{\partial x_j} \right) > 0$

* Displacement $u_i = y_i - x_i$

* Particle velocity: $v_i = \frac{\partial y_i}{\partial t} \Big|_{\underline{x}} = \frac{\partial u_i}{\partial t} \Big|_{\underline{x}}$

* Particle acceleration $a_i = \frac{\partial v_i}{\partial t} \Big|_{\underline{x}} = \frac{\partial^2 u_i}{\partial t^2} \Big|_{\underline{x}}$

We can express pos, vel, accel as functions of \underline{x} or \underline{y}

$U(\underline{x})$, $V(\underline{x})$, $a(\underline{x})$ - Lagrangean

$U^s(\underline{y})$, $V^s(\underline{y})$, $a^s(\underline{y})$ - Eulerian

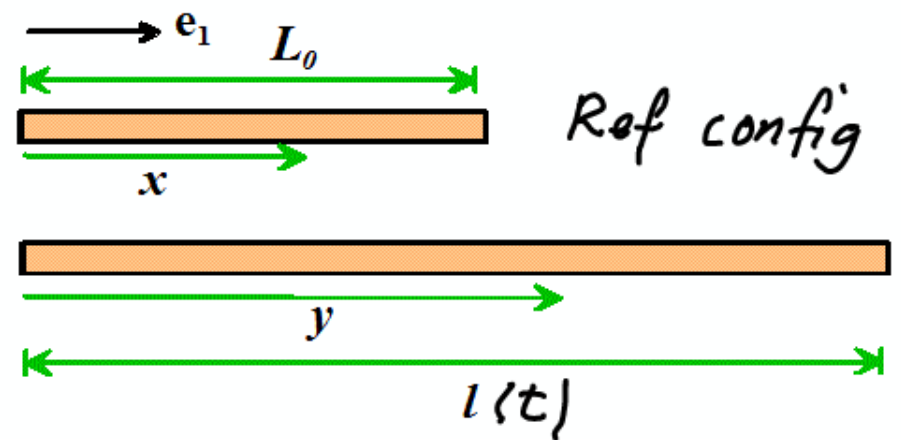
Example: 1D stretch

$$y = \frac{x}{L} \ell \Rightarrow u = x \left(\frac{\ell}{L} - 1 \right)$$

$$v = \frac{x}{L} \frac{d\ell}{dt} \quad a = \frac{x}{L} \frac{d^2\ell}{dt^2}$$

$$U^s = y \left(1 - \frac{L}{\ell} \right)$$

$$V^s = \frac{y}{\ell} \frac{d\ell}{dt} \quad a^s = \frac{y}{\ell} \frac{d^2\ell}{dt^2}$$



Eulerian

Eulerian displacement / vel / accel relations

$$V_i^s = \frac{\partial U_i^s}{\partial t} \Big|_y + \frac{\partial U_i^s}{\partial y_k} \underbrace{\frac{dy_k}{dt}}_{V_k^s} \quad - \text{particle vel}$$

$$\left(\delta_{ik} - \frac{\partial U_i^s}{\partial y_k} \right) V_k^s = \frac{\partial U_i^s}{\partial t} \Big|_y$$

$$\left(\mathbf{I} - \underbrace{\nabla_y}_{\text{symbol for spatial gradient}} \underline{U}^s \right) \underline{V}^s = \frac{\partial \underline{U}^s}{\partial t} \Big|_y$$

symbol for spatial gradient

$$a_i^s = \frac{\partial V_i^s}{\partial t} \Big|_y + \frac{\partial V_i^s}{\partial y_k} V_k^s$$

$$\underline{a}^s = \frac{\partial \underline{V}^s}{\partial t} \Big|_y + \left(\nabla_y \underline{V}^s \right) \underline{V}^s$$

Deformation Gradient

Define $F_{ij} = \frac{\partial y_i}{\partial x_j}$

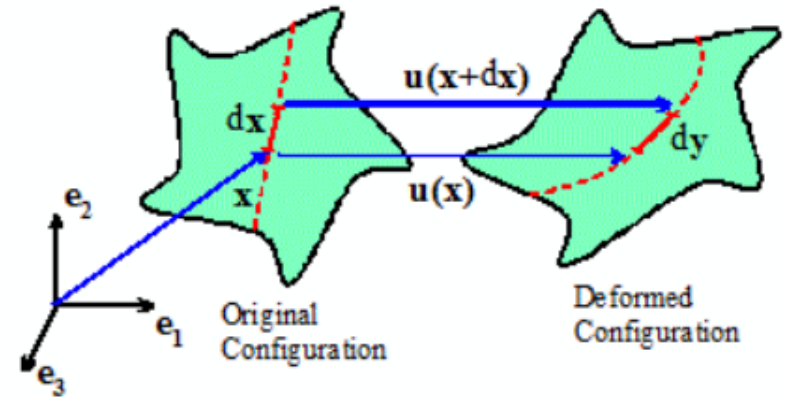
$$F = \nabla \underline{y} = \mathbf{I} + \nabla \underline{u}$$

Let \underline{dx} be a material segment in ref config
 \underline{dy} " " " " current "

$$\underline{dy} = F \underline{dx} \qquad dy_i = F_{ij} dx_j$$

To see this note

$$\underline{dy} = \underline{y}(\underline{x} + \underline{dx}) - \underline{y}(\underline{x}) = \nabla \underline{y} \underline{dx} + O(|\underline{dx}|^2)$$

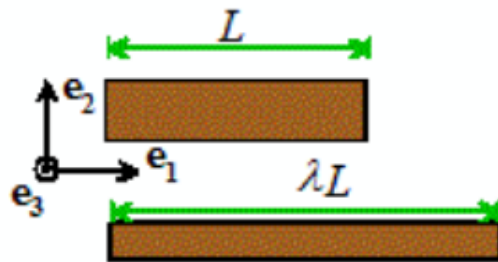


● Volume preserving uniaxial extension

$$y_1 = \lambda x_1$$

$$y_2 = x_2 / \sqrt{\lambda}$$

$$y_3 = x_3 / \sqrt{\lambda}$$



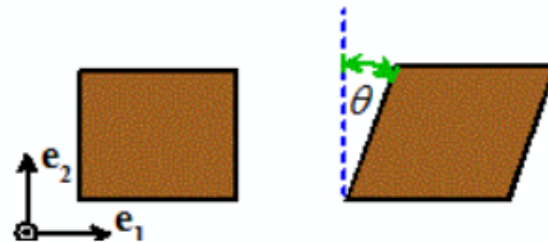
$$F = \begin{bmatrix} \lambda & 0 & 0 \\ 0 & 1/\sqrt{\lambda} & 0 \\ 0 & 0 & 1/\sqrt{\lambda} \end{bmatrix}$$

● Simple shear

$$y_1 = x_1 + \tan \theta x_2$$

$$y_2 = x_2$$

$$y_3 = x_3$$

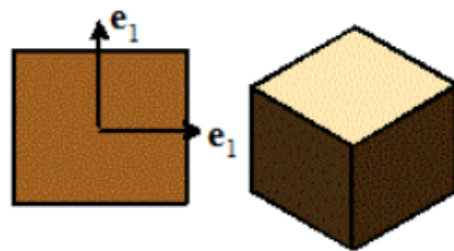


$$F = \begin{bmatrix} 1 & \tan \theta & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

● General rigid rotation about the origin

$$y = \mathbf{R} \cdot \mathbf{x} \quad \text{or} \quad y_i = R_{ij} x_j$$

where \mathbf{R} must satisfy $\mathbf{R} \cdot \mathbf{R}^T = \mathbf{R}^T \cdot \mathbf{R} = \mathbf{I}$, $\det(\mathbf{R}) > 0$. (i.e. \mathbf{R} is proper orthogonal). \mathbf{I} is the identity tensor with components $\delta_{ik} = \begin{cases} 1, & i = k \\ 0, & i \neq k \end{cases}$



$$F = \mathbf{R}$$

Use Rodriguez representation

● General homogeneous deformation

$$y_1 = A_{11}x_1 + A_{12}x_2 + A_{13}x_3 + c_1$$

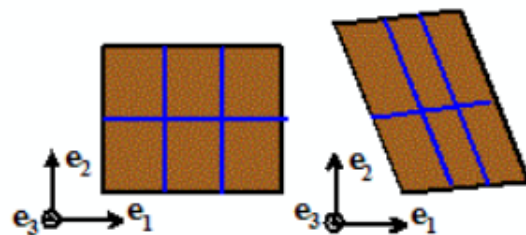
$$y_2 = A_{21}x_1 + A_{22}x_2 + A_{23}x_3 + c_2$$

$$y_3 = A_{31}x_1 + A_{32}x_2 + A_{33}x_3 + c_3$$

or

$$\mathbf{y} = \mathbf{A} \cdot \mathbf{x} + \mathbf{c} \quad y_i = A_{ij}x_j + c_i$$

where A_{ij} are constants.



$$F = \mathbf{A}$$

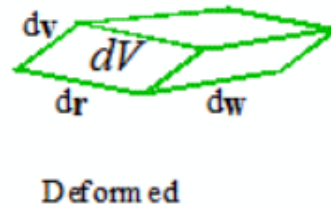
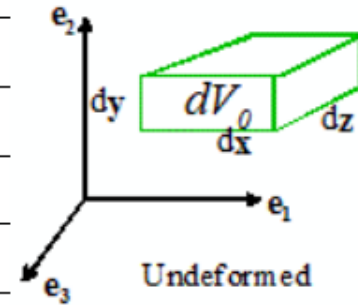
where \mathbf{A} is independent of \underline{x}

Properties of F

Jacobian: $J = \det(F)$

Relates vol element $d\vec{V}_0$ in ref config to dV in current config

$$J = \frac{dV}{d\vec{V}_0}$$



Proof $d\vec{V}_0 = d\vec{z} \cdot (d\vec{x} \times d\vec{y}) = dz_i \epsilon_{ijk} dx_j dy_k$

$$\begin{aligned} dV &= d\vec{w} \cdot (d\vec{r} \times d\vec{v}) = F_{ip} dz_p \epsilon_{ijk} F_{jq} dx_q F_{kr} dy_r \\ &= \epsilon_{pqr} \det(F) dz_p dx_q dy_r \\ &= \det(F) d\vec{V}_0 \end{aligned}$$