



School of Engineering  
Brown University

# EN40: Dynamics and Vibrations

## Final Examination

Sat May 12 2018: 9am-12:00pm

NAME: \_\_\_\_\_

### General Instructions

- No collaboration of any kind is permitted on this examination.
- You may bring 2 double sided pages of reference notes. No other material may be consulted
- Write all your solutions in the space provided. No sheets should be added to the exam.
- Make diagrams and sketches as clear as possible, and show all your derivations clearly. Incomplete solutions will receive only partial credit, even if the answer is correct.
- If you find you are unable to complete part of a question, proceed to the next part.

### Please initial the statement below to show that you have read it

By affixing my name to this paper, I affirm that I have executed the examination in accordance with the Academic Honor Code of Brown University. **PLEASE WRITE YOUR NAME ABOVE ALSO!**

\_\_\_\_\_

1-20 [40 points] \_\_\_\_\_

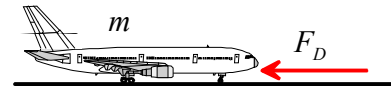
21 [10 POINTS] \_\_\_\_\_

22 [10 POINTS] \_\_\_\_\_

TOTAL [60 POINTS] \_\_\_\_\_

**FOR PROBLEMS 1-20 WRITE YOUR ANSWER IN THE SPACE PROVIDED. ONLY THE ANSWER APPEARING IN THE SPACE PROVIDED WILL BE GRADED. ILLEGIBLE ANSWERS WILL NOT RECEIVE CREDIT.**

1. The aircraft shown in the figure has mass  $m$ . While landing, it touches down with speed  $v_0$  and it is slowed by a drag force with magnitude  $F_D = cv^2$ , where  $c$  is a constant and  $v$  is the aircraft's speed. The engine thrust is negligible. The time required for the speed to decrease to  $v_0 / 2$  is given by:



- (a)  $m / (cv_0)$
- (b)  $m / (2cv_0)$
- (c)  $2m / (cv_0)$
- (d) None of the above

$$\text{Newton's law gives } -cv^2 = m \frac{dv}{dt} \Rightarrow \int_{v_0}^{v_0/2} \frac{dv}{v^2} = -\int_0^t \frac{c}{m} dt \Rightarrow \left[ \frac{1}{v} \right]_{v_0}^{v_0/2} = \frac{c}{m} t \Rightarrow t = \frac{m}{cv_0}$$

ANSWER \_\_\_\_\_ A \_\_\_\_\_ (2 POINTS)

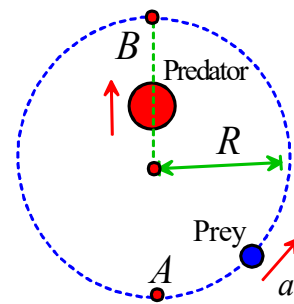
2. An aircraft with mass 1000kg gliding without engine power at constant airspeed of 50m/s takes 1 hour to descend 3600m. The drag force on the aircraft is (approximately):

- (a) 20N
- (b) 200N
- (c) 10000N
- (d) None of the above

The net rate of work done on the aircraft is zero. The power equation gives  $P_{gravity} + P_{drag} + P_{Lift} + P_{Engine} = 0$ . For this problem the engine power is zero and the lift force is workless,  $P_{gravity} = mgv_y = 1000 \times 10 \times 3600 / (1 \times 3600) = 10000$  Watts, and the rate of work done by the drag force is  $-F_D v$  where  $v$  is the airspeed. It follows that  $F_D = 10000 / 50 = 200N$

ANSWER \_\_\_\_\_ B \_\_\_\_\_ (2 POINTS)

3. A 'prey' particle starts at rest at A at time  $t=0$  and for  $t>0$  moves around a circular path with constant tangential acceleration  $a_t$ . A 'predator' starts at rest at the center of the circle at  $t=0$  and for  $t>0$  moves with constant acceleration along a vertical straight-line path. To catch the prey (i.e. to arrive at B at the same time as the prey), the predator's acceleration must be

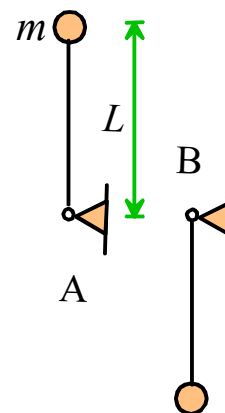


- (a)  $a_t / 2$
- (b)  $a_t$
- (c)  $a_t / \pi$
- (d)  $a_t / (2\pi)$
- (e) None of the above

The distance traveled by the prey is related to its acceleration by  $s = a_t t^2 / 2$ . To reach B it travels a distance  $\pi R$ . The distance traveled by the predator is related to its acceleration by  $s = at^2 / 2$ . To reach B it travels a distance  $R$ . For the two to reach B at the same time  $a = a_t / \pi$

ANSWER \_\_\_\_\_ C \_\_\_\_\_ (2 POINTS)

4. The pendulum shown in the figure starts at rest in the inverted vertical configuration (A) at time  $t=0$ . Following a small disturbance it falls over. At the instant when it swings through the vertical configuration (B), the magnitude of the acceleration of the mass  $m$  is (in terms of gravitational acceleration  $g$ )

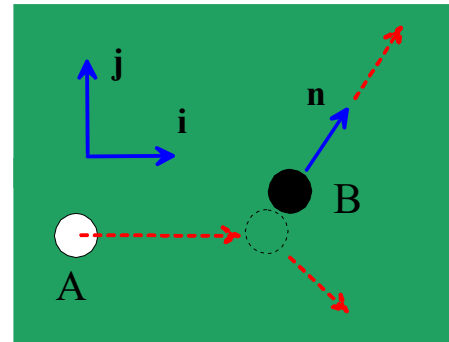


- (a) zero
- (b)  $g$
- (c)  $1.5g$
- (d)  $2g$
- (e) None of the above

Energy conservation gives  $mV^2 / 2 = mg(2L)$  (since the height of the mass decreases by  $2L$ ) so the speed of the mass is  $\sqrt{4Lg}$ . At the bottom of the swing the tangential acceleration of the mass is zero, and the normal acceleration is  $V^2 / R = 4Lg / L = 4g$

ANSWER \_\_\_\_\_ E \_\_\_\_\_ (2 POINTS)

5. A frictionless collision takes place between two billiard balls. Before impact the black ball (B) is stationary and the white one (A) has velocity  $V_0\mathbf{i}$ . The normal vector parallel to the collision direction is  $\mathbf{n} = (\mathbf{i} + \mathbf{j})/\sqrt{2}$  and the restitution coefficient for the collision is  $e = 1$ . After impact, the black ball has speed  $V_0/\sqrt{2}$ . The velocity vector of A after impact is



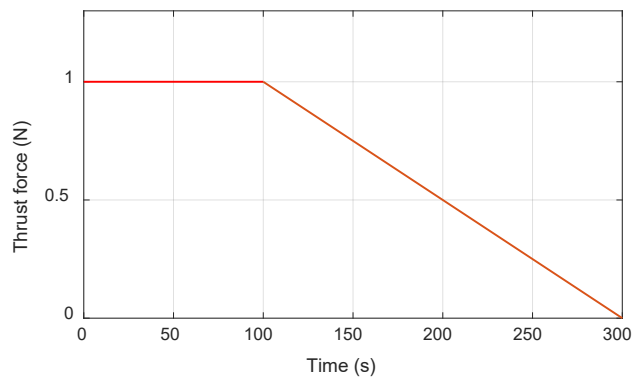
- (a) Zero
- (b)  $V_0(\mathbf{i} - \mathbf{j})/\sqrt{2}$
- (c)  $V_0(\mathbf{i} - \mathbf{j})/2$
- (d)  $V_0(\mathbf{i}\{\sqrt{2} - 1\} - \mathbf{j})/\sqrt{2}$
- (e) None of the above

Total momentum is conserved so  $mV_0\mathbf{i} = m\mathbf{v}^{A1} + mV_0(\mathbf{i} + \mathbf{j})/(\sqrt{2}\sqrt{2}) \Rightarrow \mathbf{v}^{A1} = V_0(\mathbf{i} - \mathbf{j})/2$  (you can do the same calculation with the restitution coefficient but that takes longer....)

ANSWER \_\_\_\_\_ C \_\_\_\_\_ (2 POINTS)

6. The figure shows the thrust force exerted by a model rocket motor as a function of time. The total impulse exerted by the motor is

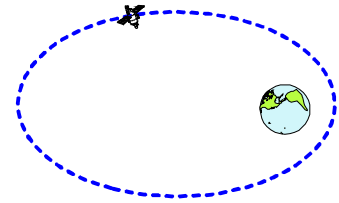
- (a) 300 Ns
- (b) 250 Ns
- (c) 200 Ns
- (d) 150 Ns
- (e) None of the above



The impulse is the area under the graph, i.e. 200N-s

ANSWER \_\_\_\_\_ C \_\_\_\_\_ (2 POINTS)

7. The figure shows a satellite in orbit around the earth. For a system consisting of only the satellite (idealized as a particle), identify whether each statement below is true or false



(a) Linear momentum is conserved

TRUE  FALSE

(b) Kinetic energy is conserved

TRUE  FALSE

(c) Potential energy is conserved

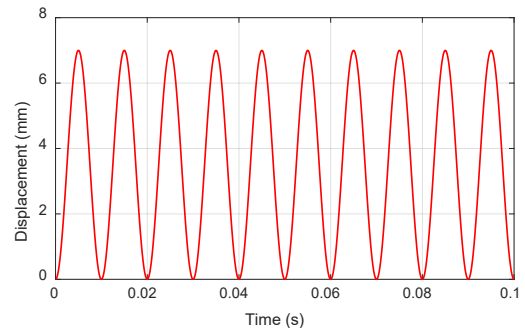
TRUE  FALSE

(d) Angular momentum about the earth's center is conserved

TRUE FALSE

8. The figure shows a vibration signal from a displacement transducer. The amplitude of the acceleration is

- (a)  $2760 \text{ m/s}^2$
- (b)  $1380 \text{ m/s}^2$
- (c)  $4.39 \text{ m/s}^2$
- (d)  $2.20 \text{ m/s}^2$
- (e) None of the above

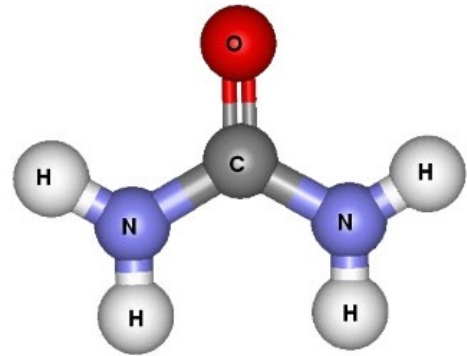


The period is 0.01s, so the angular frequency is  $200\pi \text{ rad/s}$ . The amplitude is 3.5 mm. The acceleration amplitude is therefore  $(200\pi)^2 \times 3.5 \text{ mm} / \text{s}^2 = 1380 \text{ m} / \text{s}^2$

ANSWER \_\_\_\_\_ B \_\_\_\_\_ (2 POINTS)

9. How many vibration modes does the urea molecule shown in the figure have?

- (a) 10
- (b) 18
- (c) 23
- (d) 24
- (e) None of the above



There are 8 atoms with 3 DOF each, and 6 rigid body modes. # modes = 24-6=18.

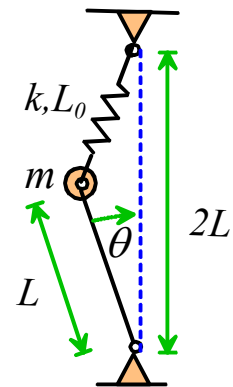
ANSWER \_\_\_\_\_ B \_\_\_\_\_ (2 POINTS)

10. The equation of motion for the system shown in the figure is

$$mL^2 \frac{d^2\theta}{dt^2} + kL^2 \left( 1 - \frac{L_0}{\sqrt{5L^2 - 4L^2 \cos\theta}} \right) \sin 2\theta - mgL \sin \theta = 0$$

The natural frequency of small amplitude vibrations of the system is

- (a)  $\sqrt{\frac{k}{m} \left( 1 - \frac{L_0}{L} \right) - \frac{g}{L}}$
- (b)  $\sqrt{\frac{2k}{m} \left( 1 - \frac{L_0}{L} \right) - \frac{g}{L}}$
- (c)  $\sqrt{\frac{2k}{m} \left( 1 - \frac{L_0}{5L} \right) - \frac{g}{L}}$
- (d)  $\sqrt{\frac{k}{m} \left( 1 - \frac{L_0}{5L} \right) - \frac{g}{L}}$
- (e) None of the above.

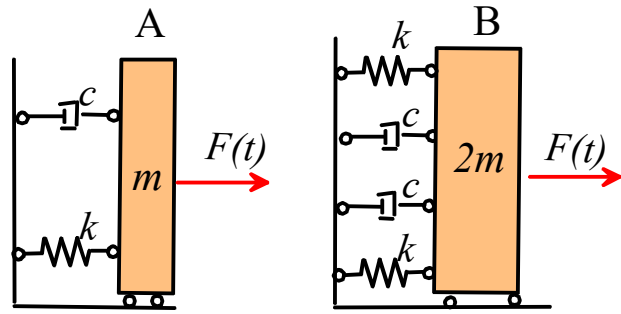


We can use the approximations  $\sin(x) \approx x, \cos(x) \approx 1$  to get a linearized EOM

$$mL^2 \frac{d^2\theta}{dt^2} + 2kL^2 \left( 1 - \frac{L_0}{L} \right) \theta - mgL\theta = 0 \Rightarrow \frac{mL^2}{2kL^2 \left( 1 - \frac{L_0}{L} \right) - mgL} \frac{d^2\theta}{dt^2} + \theta = 0 \Rightarrow \omega_n = \sqrt{\frac{2k}{m} \left( 1 - \frac{L_0}{L} \right) - \frac{g}{L}}$$

ANSWER \_\_\_\_\_ B \_\_\_\_\_ (2 POINTS)

11. Systems A and B in the figure shown are subjected to the same harmonic force  $F(t)$ . The steady state amplitude of vibration of system A is measured to be 1mm. The steady-state vibration amplitude of system B is

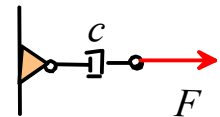


- (a) 0.5mm
- (b) 1mm
- (c) 2mm
- (d) Cannot be determined without more information
- (e) None of the above

Both systems have the same natural frequency and damping coefficient. Recall the vibration amplitude is  $X_0 = KF_0M(\omega / \omega_n, \zeta)$  where  $K = 1/k_{eff}$ . Since  $\omega_n, \zeta$  are equal for A,B,  $M$  does not change. The effective stiffness of B is twice that of A, the amplitude of vibration of B will be half that of A

ANSWER \_\_\_\_\_ A \_\_\_\_\_ (2 POINTS)

12. A dashpot is stretched by a constant force  $F$  as shown in the figure. The rate of work done by the force is



- (a)  $cF$
- (b)  $F / c$
- (c)  $F^2 / c$
- (d)  $cF^2$
- (e) None of the above

The force moves with speed  $F / c$  (from the force-stretch rate formula for a dashpot). The rate of work done is  $Fv = F^2 / c$ .

ANSWER \_\_\_\_\_ C \_\_\_\_\_ (2 POINTS)

13. A rigid body is subjected to a sequence of two rotations.

$$\mathbf{R}^{(1)} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & -1 & 0 \end{bmatrix} \quad \mathbf{R}^{(2)} = \begin{bmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

The sequence of rotations  $\mathbf{R} = \mathbf{R}^{(2)}\mathbf{R}^{(1)}$  represents

- (a) A 120 degree rotation about an axis parallel to  $\mathbf{n} = (-\mathbf{i} + \mathbf{j} - \mathbf{k}) / \sqrt{3}$
- (b) A 30 degree rotation about an axis parallel to  $\mathbf{n} = (-\mathbf{i} + \mathbf{j} - \mathbf{k}) / \sqrt{3}$
- (c) A 45 degree rotation about an axis parallel to  $\mathbf{k}$
- (d) A 45 degree rotation about an axis parallel to  $\mathbf{i}$
- (e) None of the above.

The two rotations yield a matrix

$$\mathbf{R} = \begin{bmatrix} 0 & 0 & 1 \\ -1 & 0 & 0 \\ 0 & -1 & 0 \end{bmatrix}$$

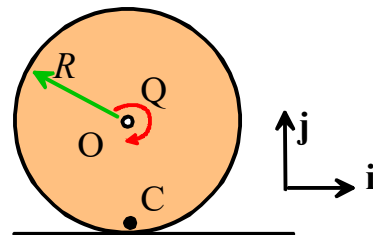
The formula gives  $1 + 2 \cos \theta = R_{xx} + R_{yy} + R_{zz} = 0 \Rightarrow \cos \theta = -1/2 \Rightarrow \theta = 120^\circ$

$$\mathbf{n} = [(R_{zy} - R_{yz})\mathbf{i} + (R_{xz} - R_{zx})\mathbf{j} + (R_{yx} - R_{xy})\mathbf{k}] / 2 \sin \theta = (-\mathbf{i} + \mathbf{j} - \mathbf{k}) / \sqrt{3}$$

ANSWER \_\_\_\_\_ A \_\_\_\_\_ (2 POINTS)

14. The center of the wheel moves with (instantaneous) velocity  $\mathbf{v}_O = V\mathbf{i}$  and the wheel rolls without slip. A torque  $\mathbf{Q} = -Q\mathbf{k}$  is exerted on the wheel by an axle attached to O. The rate of work done by the torque on the wheel is:

- (a) Zero
- (b)  $QV$
- (c)  $QV/R$
- (d)  $QVR$
- (e) None of the above

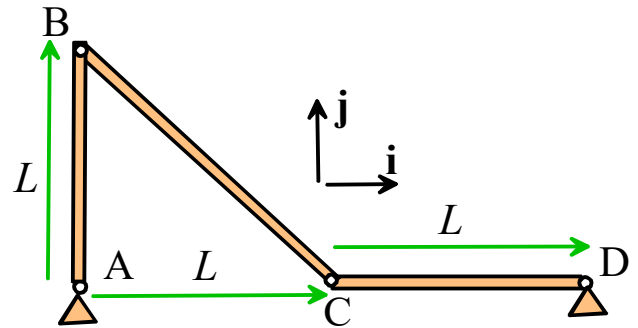


The rolling wheel formula gives the angular velocity as  $\omega = -V/R$ . The rate of work done by the torque is  $\mathbf{Q} \cdot \boldsymbol{\omega} = QV/R$ .

ANSWER \_\_\_\_\_ C \_\_\_\_\_ (2 POINTS)



15. Member AB in the four-bar mechanism shown in the figure rotates with constant angular velocity  $\omega_{AB} = \omega_0 \mathbf{k}$ . At the instant shown, the angular velocity and angular acceleration of member BC are



- (a)  $\omega_{BC} = \omega_0 \mathbf{k}$   $\alpha_{BC} = 2\omega_0^2 \mathbf{k}$
- (b)  $\omega_{BC} = \omega_0 \mathbf{k}$   $\alpha_{BC} = -2\omega_0^2 \mathbf{k}$
- (c)  $\omega_{BC} = -\omega_0 \mathbf{k}$   $\alpha_{BC} = \omega_0^2 \mathbf{k}$
- (d)  $\omega_{BC} = \omega_0 \mathbf{k}$   $\alpha_{BC} = \mathbf{0}$
- (e) None of the above

The kinematics equations give  $\mathbf{v}_B = \omega_0 \mathbf{k} \times L \mathbf{j}$ ;  $\mathbf{v}_C - \mathbf{v}_B = \omega_{BC} \mathbf{k} \times L(\mathbf{i} - \mathbf{j})$   $\mathbf{v}_D - \mathbf{v}_C = \omega_{CD} \mathbf{k} \times L \mathbf{i}$ . Adding and noting  $\mathbf{v}_D = \mathbf{0}$   $L \mathbf{k} \times (\omega_0 \mathbf{j} + \omega_{BC}(\mathbf{i} - \mathbf{j}) + \omega_{CD} \mathbf{i}) = \mathbf{0} \Rightarrow \omega_{BC} = \omega_0, \omega_{CD} = -\omega_0$

For accelerations  $\mathbf{a}_B = -\omega_0^2 L \mathbf{j}$ ;  $\mathbf{a}_C - \mathbf{a}_B = \alpha_{BC} \mathbf{k} \times L(\mathbf{i} - \mathbf{j}) + \omega_0^2 L(-\mathbf{i} + \mathbf{j})$   $\mathbf{a}_D - \mathbf{a}_C = \alpha_{CD} \mathbf{k} \times L \mathbf{i} - \omega_0^2 L \mathbf{i}$

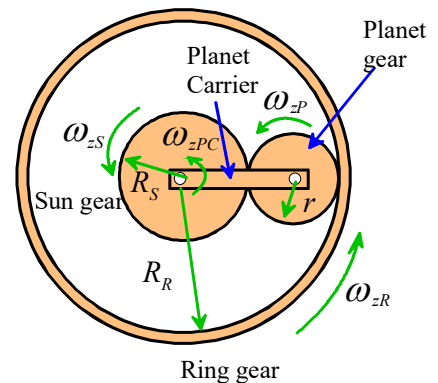
Expand and add  $\mathbf{a}_D = -\omega_0^2 L \mathbf{j} + \alpha_{BC} L(\mathbf{j} + \mathbf{i}) + \omega_0^2 L(-\mathbf{i} + \mathbf{j}) + \alpha_{CD} L \mathbf{j} - \omega_0^2 L \mathbf{i} = \mathbf{0} \Rightarrow \alpha_{BC} = 2\omega_0^2$

ANSWER      A      (2 POINTS)

16. With the sun gear fixed, the planet carrier and ring gears in the epicyclic gear system shown have a ratio  $\omega_{zR} / \omega_{zPC} = 3 / 2$ .

If the sun gear has 20 teeth, the ring and planet gears have

- (a)  $N_R = 40, N_P = 10$  teeth
- (b)  $N_R = 40, N_P = 20$  teeth
- (c)  $N_R = 80, N_P = 20$  teeth
- (d)  $N_R = 80, N_P = 30$  teeth
- (e) None of the above



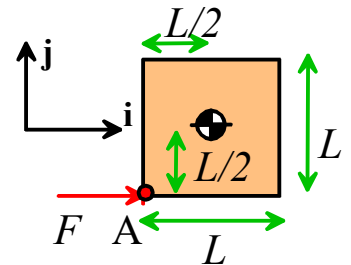
The general formula relating angular velocities in a planetary gear system is  $(\omega_{zR} - \omega_{zPC}) / (\omega_{zS} - \omega_{zPC}) = -(N_S / N_R)$

Substituting numbers given

$$(3\omega_{zPC} - 2\omega_{zPC}) / (0 - 2\omega_{zPC}) = -20 / N_R \Rightarrow N_R = 40. \text{ Finally } 2N_P = N_R - N_S \Rightarrow N_P = 10$$

ANSWER      A      (2 POINTS)

17. A square plate with mass  $m$ , side length  $L$ , and mass moment of inertia  $mL^2 / 12$  is at rest for time  $t < 0$ . At time  $t = 0$  a force  $F$  is applied at the corner located at point A in the figure. At the instant  $t = 0$  the acceleration vector of point A is

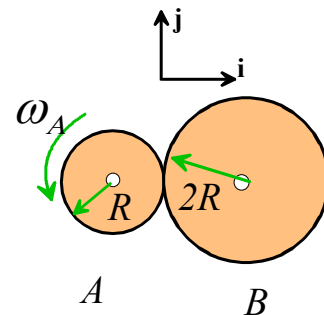


- (a)  $\mathbf{a} = (F / m)\mathbf{i}$
- (b)  $\mathbf{a} = 3(F / m)\mathbf{i}$
- (c)  $\mathbf{a} = 4(F / m)\mathbf{i} - 3(F / m)\mathbf{j}$
- (d)  $\mathbf{a} = 3(F / m)\mathbf{i} - 3(F / m)\mathbf{j}$
- (e) None of the above

The mass moment of inertia of the plate is  $I_{Gzz} = mL^2 / 12$  (given). Taking moments about the center of the plate, the equations of motion are  $F\mathbf{i} = m\mathbf{a}_G$   $(FL / 2)\mathbf{k} = I_{Gzz}\alpha\mathbf{k} \Rightarrow \alpha = 6F / (mL)$ . The acceleration of point A is  $\mathbf{a}_A = \mathbf{a}_G + \alpha\mathbf{k} \times (-L/2)\mathbf{i} - (L/2)\mathbf{j} = (F / m)\mathbf{i} + (3F / m)\mathbf{i} - 3(F / m)\mathbf{j}$

ANSWER \_\_\_\_\_ C \_\_\_\_\_ (2 POINTS)

18. The two gears A and B in the figure have radii  $R$  and  $2R$ , and mass moments of inertia  $mR^2 / 2$  and  $2mR^2$ , respectively. Their centers are stationary. If gear A rotates counterclockwise at angular speed  $\omega_A$ , the total angular momentum of the system (including both gears) is



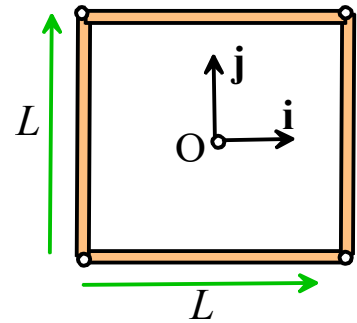
- (a) zero
- (b)  $(mR^2)\omega_A\mathbf{k}$
- (c)  $-(mR^2 / 2)\omega_A\mathbf{k}$
- (d)  $(3mR^2 / 2)\omega_A\mathbf{k}$
- (e) None of the above

The total angular momentum is  $(I_{Azz}\boldsymbol{\omega}_A + I_{Bzz}\boldsymbol{\omega}_B)$ ; we know  $\omega_B = -\omega_A R_A / R_B = -\omega_A / 2$  and so the total angular momentum is  $((mR^2 / 2)\omega_A - 2mR^2\omega_A / 2)\mathbf{k} = -mR^2\omega_A / 2$

ANSWER \_\_\_\_\_ C \_\_\_\_\_ (2 POINTS)

19. Four rods with mass  $m$  and length  $L$  are connected to form a square frame as shown in the figure. The mass moment of inertia of the frame about its center is

- (a)  $4mL^2 / 3$
- (b)  $5mL^2 / 6$
- (c)  $3mL^2 / 2$
- (d)  $5mL^2 / 6$
- (e) None of the above

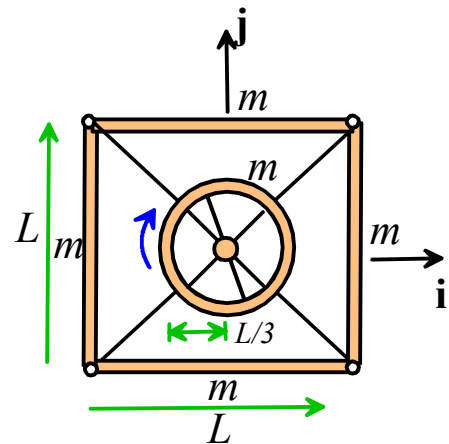


The mass moment of inertia of a bar with length  $L$  is  $mL^2 / 12$ . Using the parallel axis theorem the total mass moment of inertia is  $4 \left( \frac{mL^2}{12} + m \left( \frac{L}{2} \right)^2 \right) = 4mL^2 / 3$

ANSWER \_\_\_\_\_ A \_\_\_\_\_ (2 POINTS)

20. A spacecraft is idealized as a frame made up of 4 bars with length  $L$  and mass  $m$ . The orientation of the spacecraft is controlled by a momentum wheel that can be idealized as a thin ring with mass  $m$  and radius  $R=L/3$ . At time  $t=0$  the spacecraft is at rest (in space) and the momentum wheel is stationary. A motor then spins up the momentum wheel to an angular velocity  $-\omega_0 \mathbf{k}$  (relative to the frame). The angular speed of the frame is

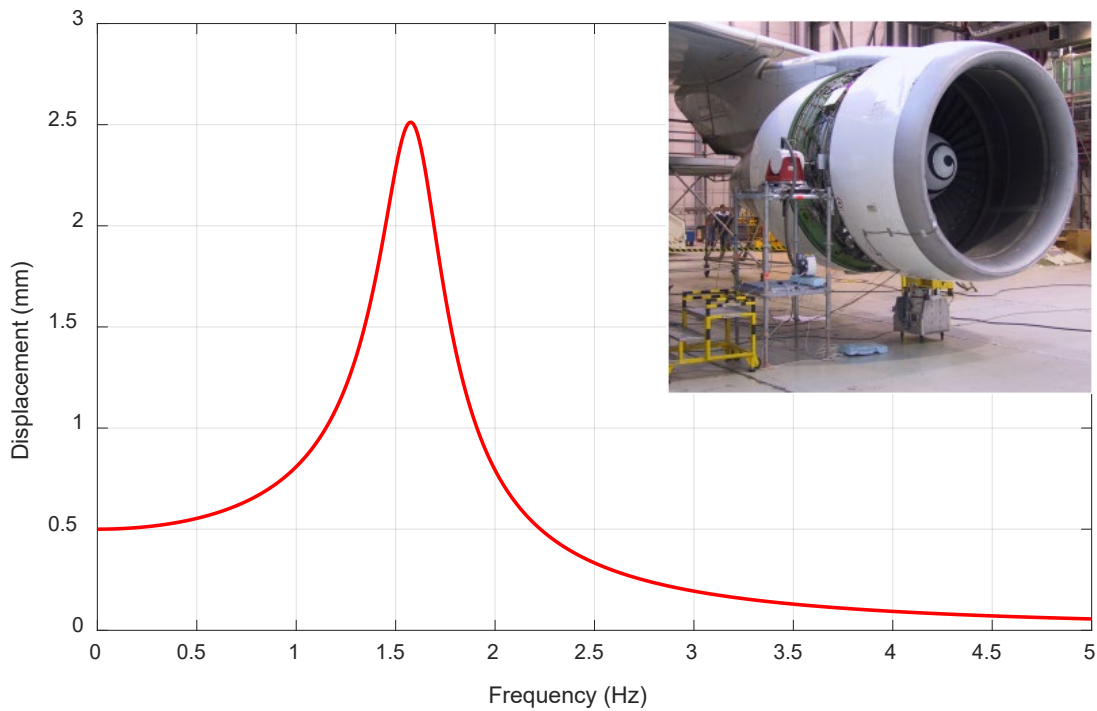
- (a)  $\omega_f = (\omega_0 / 10) \mathbf{k}$
- (b)  $\omega_f = (\omega_0 / 11) \mathbf{k}$
- (c)  $\omega_f = (\omega_0 / 12) \mathbf{k}$
- (d)  $\omega_f = (\omega_0 / 13) \mathbf{k}$
- (e) None of the above



Since no external forces or torques act on the system, angular momentum of the frame + momentum wheel is conserved. Since the initial angular momentum is zero this requires

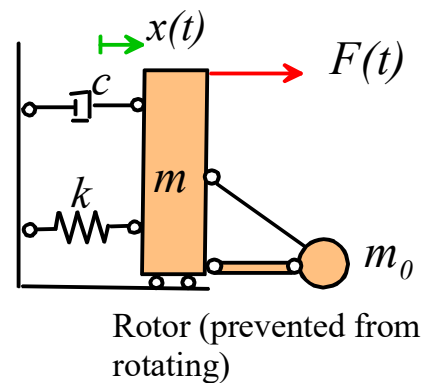
$$(4mL^2 / 3)\omega_f \mathbf{k} + m(L/3)^2(-\omega_0 + \omega_f) \mathbf{k} = 0 . \text{ Therefore } \omega_f = \omega_0 / 13$$

ANSWER \_\_\_\_\_ D \_\_\_\_\_ (2 POINTS)



21 As part of the airworthiness certification process, the rotating parts of a jet engine are prevented from turning, and the engine is subjected to an external horizontal harmonic force  $F(t) = F_0 \sin \omega t$  with amplitude  $F_0 = 250\text{N}$ . The amplitude  $X_0$  of the steady-state horizontal vibration  $x(t) = X_0 \sin(\omega t + \phi)$  of the engine is measured.

The measured displacement amplitude  $X_0$  is shown in the figure as a function of frequency (in cycles/sec).



21.1 Assuming that the engine and its mounting are idealized as a spring-mass-damper system (with light damping), use the graph provided to estimate values for the following quantities

- (a) The natural frequency of vibration of the engine (give both the frequency in cycles per second and the angular frequency)

From the graph,  $f_n = 1.6\text{Hz}$ ;  $\omega_n = 2\pi f_n = 10\text{rad / s}$

[2 POINTS]

- (b) The damping factor  $\zeta$ . (Use the peak. Note that the graph shows the displacement amplitude, not magnification  $M$ )

We can get  $\zeta$  from the peak. The magnification is  $2.5/0.5=5$ , and we know  $M \approx 1/2\zeta \Rightarrow \zeta = 0.1$

[2 POINTS]

(c) The spring stiffness (use the displacement at very low frequency)

We can get the stiffness from the zero frequency deflection (static).

$$k = F / X_0 \Rightarrow k = 250 / 0.5 \times 10^{-3} = 500 \text{ kN} / \text{m}$$

[1 POINT]

(d) The total mass  $m + m_0$

The mass follows from the natural frequency  $\sqrt{k / (m + m_0)} = \omega_n \Rightarrow m + m_0 = k / \omega_n^2 = 5000 \text{ kg}$

[1 POINT]

(e) The dashpot coefficient  $c$

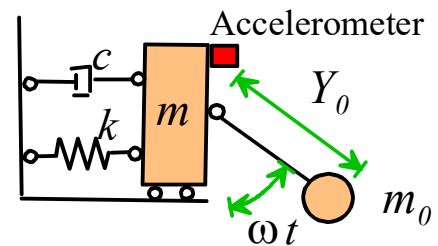
Using the formula:  $\zeta = c / 2\sqrt{k(m + m_0)} \Rightarrow c = 10 \text{ kNs} / \text{m}$

[1 POINT]

21.2 During operation, the engine spins at 9550 rpm. An accelerometer mounted on the outside of the engine measures a harmonic acceleration with amplitude  $10 \text{ m/s}^2$ . What is the amplitude of the displacement?

The vibration is harmonic, therefore

$$X_0 = A_0 / \omega^2 = 10 / (9550 \times 2\pi / 60)^2 = 0.01 \text{ mm}$$



[1 POINT]

21.3 What is the engine speed (in rpm) at which the steady-state displacement amplitude will be a maximum?

The maximum vibration amplitude will occur when the engine spins at the resonant frequency; this corresponds to  $1.6 \times 60 = 96 \text{ rpm}$

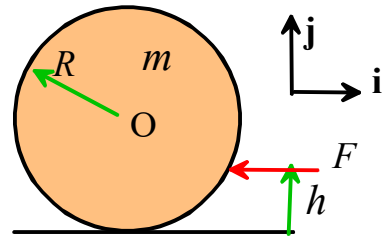
[1 POINT]

21.4 What is the steady-state displacement amplitude when the engine runs at the speed in 21.3?

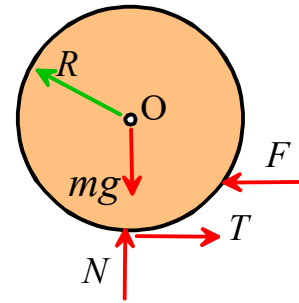
During operation the engine spins much faster than the resonant frequency. We know the magnification is approximately 1 in this regime, and we know the amplitude is 0.01mm from 21.2. At resonance, the magnification is 5. We expect a vibration amplitude of 0.05mm.

**[1 POINT]**

22. The figure shows a spherical billiard ball with mass  $m$  and radius  $R$  at rest on a pool table. It is subjected to a horizontal force  $F$  by a cue at a height  $h$  above the table.



2.1 Draw a free body diagram showing all the forces acting on the ball (include gravity and assume no slip at the contact)



[2 POINTS]

2.2 Write down the equations of motion (Newton's law, and the angular momentum equation)

$$\mathbf{F} = m\mathbf{a} \Rightarrow (T - F)\mathbf{i} + (N - mg)\mathbf{j} = ma_{Gx}\mathbf{i}$$

$$\begin{aligned} \sum \mathbf{r} \times \mathbf{F} + \mathbf{Q} &= \frac{d\mathbf{h}}{dt} \Rightarrow hF\mathbf{k} = R\mathbf{j} \times ma_{Gx}\mathbf{i} + I_{Gzz}\alpha_z\mathbf{k} \\ &\Rightarrow hF\mathbf{k} = -Rma_{Gx}\mathbf{k} + \frac{2}{5}mR^2\alpha_z\mathbf{k} \end{aligned}$$

[2 POINTS]

2.3 Write down the kinematics equation relating the acceleration of the center at O and the angular acceleration of the sphere

$$a_{Gx} = -R\alpha_z$$

[1 POINT]

2.4 Hence, calculate the acceleration of the sphere

Using 2.3, 2.4, note that  $hF = -Rma_{Gx} - \frac{2}{5}mRa_{Gx} \Rightarrow a_{Gx} = -\frac{5h}{7R} \frac{F}{m}$

[2 POINTS]

2.5 Calculate the reaction forces at the contact. If the coefficient of friction at the contact is  $\mu$ , find a formula for the critical value of  $F$  that will cause slip at the contact, in terms of  $m, g, h, R$ .

$(T - F)\mathbf{i} + (N - mg)\mathbf{j} = ma_{Gx}\mathbf{i}$  shows that

$$N = mg \quad T = -m \frac{5h}{7R} \frac{F}{m} + F = F \left(1 - \frac{5h}{7R}\right)$$

At the onset of slip  $|T| = \mu N \Rightarrow F \left(1 - \frac{5h}{7R}\right) = \mu mg \Rightarrow F = \mu mg / \left(1 - \frac{5h}{7R}\right)$

**[2 POINTS]**

2.6 Where should the ball be struck to guarantee no slip for any value of  $F$ ?

We can choose  $h$  to make  $T=0$ , which requires  $h = 7R / 5$

**[1 POINT]**