

1.

$$\underline{V}_B = \underline{V}_A + (\underline{\omega}_{AB} \times \underline{r}_{B/A})$$

Solutions HW 7  
Rigid Body Kin.

$$= 0 + \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 0 & 0 & 4 \\ 2 & 12 & 0 \end{vmatrix} = (-48\hat{i} + 8\hat{j}) \text{ cm/s}$$

$$\underline{V}_C = \underline{V}_B + (\underline{\omega}_{BC} \times \underline{r}_{C/B})$$

$$\underline{V}_C = (-48\hat{i} + 8\hat{j}) + \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 0 & 0 & \omega_{BC} \\ 16 & -2 & 0 \end{vmatrix}$$

$$\star \underline{V}_C = (-48 + 2\omega_{BC})\hat{i} + (8 + 16\omega_{BC})\hat{j}$$

$$\underline{V}_D = \underline{V}_C + (\underline{\omega}_{CD} \times \underline{r}_{C/D})$$

$$0 = \underline{V}_C + \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 0 & 0 & \omega_{CD} \\ 4 & 3 & 0 \end{vmatrix} = \underline{V}_C + (-3\omega_{CD})\hat{i} + 4\omega_{CD}\hat{j}$$

$$\star \underline{V}_C = 3\omega_{CD}\hat{i} - 4\omega_{CD}\hat{j} \Rightarrow \begin{matrix} 2 \text{ eqns} \\ 2 \text{ unknowns} \end{matrix}$$

$$(3\omega_{CD} = -48 + 2\omega_{BC})\hat{i}$$

$$(-4\omega_{CD} = 8 + 16\omega_{BC})\hat{j}$$

$\omega_{BC} = 3 \text{ rad/s}$
$\omega_{CD} = -14 \text{ rad/s}$

①

2.1. Front gear is rigidly attached to petals

$$\alpha_p = \alpha_1$$

$$\omega_p = \omega_1$$

Integrating  $\alpha_p = \int \ddot{\omega}_p dt$

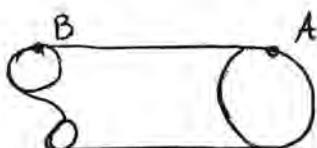
$$\begin{cases} t/2 & 0 \leq t < 2 \\ 1 & 2 \leq t < 12 \\ -t/2 + 7 & 12 \leq t \leq 14 \end{cases}$$

We obtain  $\omega_1 = \int \dot{\omega}_1 dt$

$$\begin{cases} t^2/4 & 0 \leq t < 2 \\ t - 1 & 2 \leq t < 12 \\ -t^2/4 + 7t - 37 & 12 \leq t \leq 14 \end{cases}$$

see attached for plots

2.2.



At A & B, velocities must be equal:  $v_A = v_B$

$$r_2 \omega_2 = r_1 \omega_1$$

$$\omega_2 = \left(\frac{r_1}{r_2}\right) \omega_1$$

$$\omega_2 = \frac{8}{3} \omega_1 \quad \text{see attached plot}$$

2.3. Number of Revolutions is found by integrating  $\omega_p(t)$

$$\theta_p(t) = \begin{cases} t^3/12 & 0 \leq t < 2 \\ t^2/2 - t + 2/3 & 2 \leq t < 12 \\ -t^3/12 + 7/2 t^2 - 37t + \frac{434}{3} & 12 \leq t \leq 14 \end{cases}$$
(2)

$$\theta_p(t=14 \text{ sec}) = 84 \text{ radians}$$

$$84/2\pi = 13.4 \text{ Revolutions}$$

2.4. Distance travelled is revolutions of rear wheel  $\times 2\pi r_w$  (circumference).

$$\theta_w = \theta_2 = \int \omega_2 dt \text{ and } \omega_2 = \frac{8}{3} \omega_1 \text{ so}$$

$$\theta_w(t) = \frac{8}{3} \int \omega_1 dt = \frac{8}{3} \cdot \theta_1(t)$$

$$\theta_w(t=14 \text{ sec.}) = 224 \text{ radians}$$

$$\frac{224}{2\pi} = 35.7 \text{ revolutions}$$

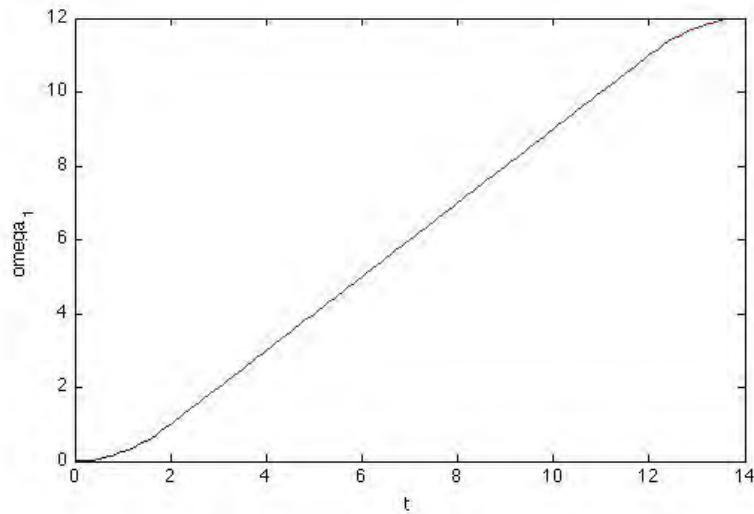
$$35.7 (2\pi r_w) = 74 \text{ meters}$$

2.5. The forward velocity is  $v_o = \omega_w r_w$

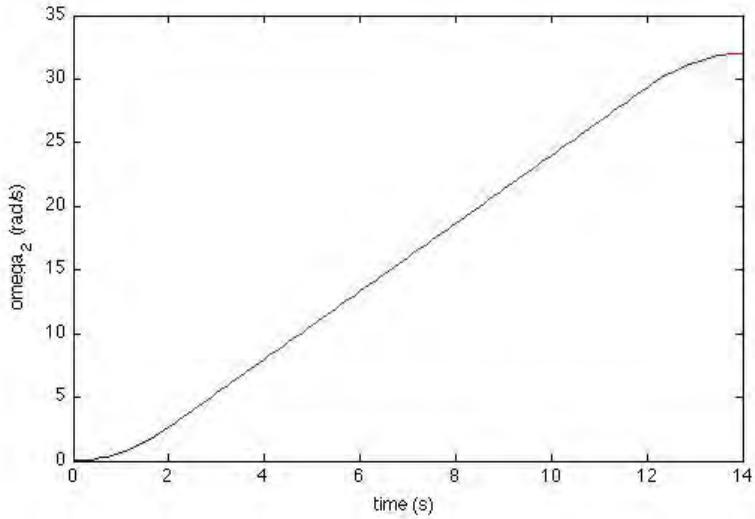
$$v_o = r_w \cdot \omega_2$$

see attached plot

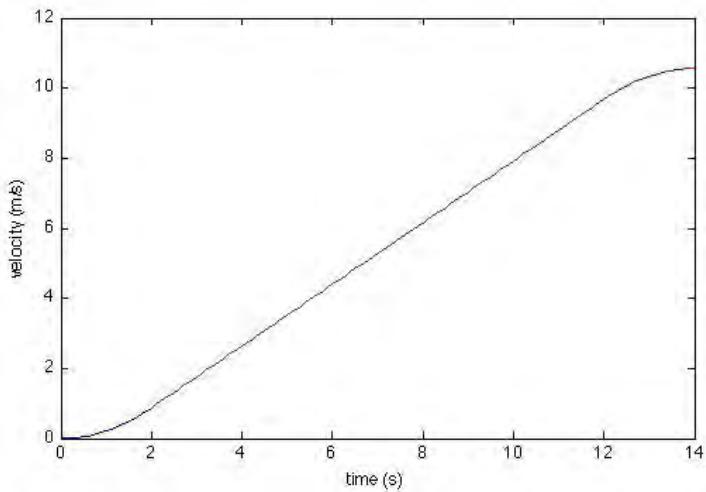
2.1



2.2



2.5



# Helmet Impact

3.1.

$$\underline{a}_1 = \underline{a}_{cm} + (\underline{\alpha} \times \underline{r}_1) + (\underline{\omega} \times (\underline{\omega} \times \underline{r}_1))$$

3.2.  $\underline{a}_1 = [\underline{a}_{cm} + (\underline{\alpha} \times \underline{r}_1) + (\underline{\omega} \times (\underline{\omega} \times \underline{r}_1))] \cdot \underline{e}_1$

3.3. Unknowns: 3 components of  $\underline{a}_{cm}$  +  
3 components of  $\underline{\alpha}$  = 6!

We need 6 equations and 6 accelerometers!

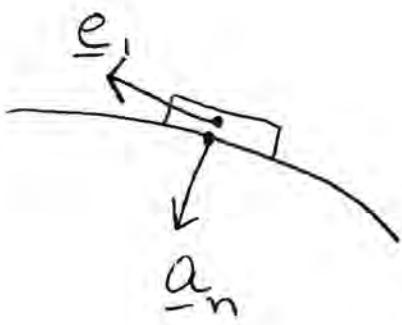
$$a_1 = \dots$$

$$a_2 = \dots$$

:

$$a_6 = \dots$$

3.4.



$$\underline{a}_t = \underline{\alpha} \times \underline{r}_1$$

$$\underline{a}_n = \underline{\omega} \times (\underline{\omega} \times \underline{r}_1)$$

If  $\underline{e}_1$  is perpendicular to  $\underline{a}_n$   
then  $\underline{e}_1 \cdot \underline{a}_n = 0$ . Thus we  
can neglect  $\underline{\omega} \times (\underline{\omega} \times \underline{r}_1)$

$$\boxed{\underline{a}_1 = [\underline{a}_{cm} + (\underline{\alpha} \times \underline{r}_1)] \cdot \underline{e}_1}$$

3.5.

$$\begin{aligned} \underline{a}_1 &= (a_x + \alpha_y r_z - \alpha_z r_y) \underline{e}_x + \\ &\quad (a_y - \alpha_x r_z + \alpha_z r_x) \underline{e}_y + \\ &\quad (a_z + \alpha_x r_y - \alpha_y r_x) \underline{e}_z \end{aligned}$$

3.6

$$\underline{A} \underline{X} = \underline{B} \quad \text{for Matlab}$$

$$\underline{X} = \begin{bmatrix} a_x \\ a_y \\ a_z \\ \alpha_x \\ \alpha_y \\ \alpha_z \end{bmatrix} \quad \underline{B} = \begin{bmatrix} a_1 \\ a_2 \\ a_3 \\ a_4 \\ a_5 \\ a_6 \end{bmatrix}$$

$\underline{A}$  =  $6 \times 6$  matrix  
of coefficients  
 $\underline{Y}_n$  &  $\underline{E}_n$  for  $n=1 \rightarrow 6$   
see attached code.

$$|\underline{a}_{cm}| = 404 \text{ m/s}^2 \quad \text{OR} \quad 41 \text{ g's}$$

$$a_x = 400 \text{ m/s}^2$$

$$a_y = -30 \text{ m/s}^2$$

$$a_z = 50 \text{ m/s}^2$$

$$\alpha = (698\hat{i} + 5000\hat{j} - 12000\hat{k}) \text{ rad/s}^2$$

HW #7 Problem #3

$$\textcircled{a} \quad \underline{r}_D = R \hat{i} + L \hat{k}$$

$$\underline{r}_E = R \cos\left(\frac{2\pi}{3}\right) \hat{i} + R \sin\left(\frac{2\pi}{3}\right) \hat{j} + L \hat{k}$$

$$\underline{r}_F = R \cos\left(\frac{4\pi}{3}\right) \hat{i} + R \sin\left(\frac{4\pi}{3}\right) \hat{j} + L \hat{k}$$

$$\textcircled{b} \quad \underline{r}_a = R \cos\theta \hat{i} + R \sin\theta \hat{j} + z \hat{k}$$

$$\underline{r}_b = R \cos\left(\frac{2\pi}{3} + \theta\right) \hat{i} + R \sin\left(\frac{2\pi}{3} + \theta\right) \hat{j} + z \hat{k}$$

$$\underline{r}_c = R \cos\left(\frac{4\pi}{3} + \theta\right) \hat{i} + R \sin\left(\frac{4\pi}{3} + \theta\right) \hat{j} + z \hat{k}$$

$$\textcircled{c} \quad \underline{r}_{AD} = \underline{r}_D - \underline{r}_a = R(1 - \cos\theta) \hat{i} - R \sin\theta \hat{j} + (L - z) \hat{k}$$

$$|\underline{r}_{AD}|^2 = L^2$$

$$\Rightarrow R^2(1 - \cos\theta)^2 + R^2 \sin^2\theta + (L - z)^2 = L^2$$

$$R^2 + R^2 \cos^2\theta - 2R^2 \cos\theta + R^2 \sin^2\theta + L^2 + z^2 - 2Lz = L^2$$

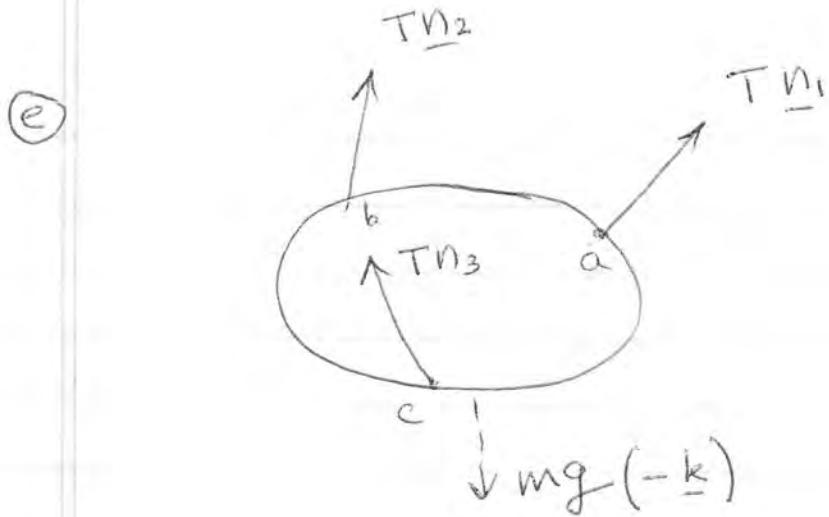
$$\Rightarrow 2R^2(1 - \cos\theta) + z(z - 2L) = 0$$

$$\cos\theta = 1 - \frac{\theta^2}{2!} + \frac{\theta^4}{4!} - \dots \quad \text{For small } \theta, \cos\theta = 1 - \frac{\theta^2}{2}$$

Also, for small values of  $\theta$ ,  $z \ll 2L \Rightarrow z - 2L \approx -2L$

$$2R^2 \frac{\theta^2}{2} - 2Lz = 0 \Rightarrow z \approx \frac{R^2 \theta^2}{2L}$$

$$\textcircled{d} \quad \underline{n}_1 = \frac{\underline{r}_D - \underline{r}_a}{L}, \quad \underline{n}_2 = \frac{\underline{r}_E - \underline{r}_b}{L}, \quad \underline{n}_3 = \frac{\underline{r}_F - \underline{r}_c}{L}$$



(f) Net Force = (acceleration of the COM) \* m

$$Tn_1 + Tn_2 + Tn_3 - mg\hat{k} = m \left[ a_x \hat{i} + a_y \hat{j} + \frac{d^2 z}{dt^2} \hat{k} \right]$$

$$\Rightarrow \frac{T}{L} \left[ (r_D + r_E + r_F) - (r_a + r_b + r_c) \right] - mg\hat{k} = m \left[ a_x \hat{i} + a_y \hat{j} + \frac{d^2 z}{dt^2} \hat{k} \right]$$

(g)  $\frac{r_a + r_b + r_c}{3} = z\hat{k}$

$$\frac{r_D + r_E + r_F}{3} = L\hat{k}$$

$$\Rightarrow m \left[ a_x \hat{i} + a_y \hat{j} + \frac{d^2 z}{dt^2} \hat{k} \right] = \frac{T}{L} \left[ 3L\hat{k} - 3z\hat{k} \right] - mg\hat{k}$$

$$= \left[ 3T \left( 1 - \frac{z}{L} \right) - mg \right] \hat{k}$$

(h) For small values of  $z$ ,  $z \approx 0$ ,  $\frac{d^2 z}{dt^2} \approx 0$

$$\Rightarrow 3T - mg = 0 \Rightarrow T = \frac{mg}{3}$$

$$\textcircled{1} \quad \sum \underline{M}_{\text{com}} = I \underline{\alpha}$$

↑ Net moment about the center of mass

$$\Rightarrow I \frac{d\theta}{dt} \underline{k} = (\underline{r}_a - z \underline{k}) \times \frac{I}{L} (\underline{r}_D - \underline{r}_a) + (\underline{r}_b - z \underline{k}) \times \frac{I}{L} (\underline{r}_E - \underline{r}_b) \\ + (\underline{r}_c - z \underline{k}) \times \frac{I}{L} (\underline{r}_F - \underline{r}_c)$$

$$= \frac{I}{L} \left[ \underline{r}_a \times (\underline{r}_D - \underline{r}_a) - z \underline{k} \times (\underline{r}_D - \underline{r}_a) + \underline{r}_b \times (\underline{r}_E - \underline{r}_b) \right. \\ \left. - z \underline{k} \times (\underline{r}_E - \underline{r}_b) + \underline{r}_c \times (\underline{r}_F - \underline{r}_c) - z \underline{k} \times (\underline{r}_F - \underline{r}_c) \right]$$

$$= \frac{I}{L} \left[ \underline{r}_a \times \underline{r}_D - \cancel{\underline{r}_a \times \underline{r}_a}^0 - z \underline{k} \times \underline{r}_D + z \underline{k} \times \underline{r}_a + \underline{r}_b \times \underline{r}_E \right. \\ \left. - \cancel{\underline{r}_b \times \underline{r}_b}^0 - z \underline{k} \times \underline{r}_E + z \underline{k} \times \underline{r}_b + \underline{r}_c \times \underline{r}_F - \cancel{\underline{r}_c \times \underline{r}_c}^0 \right. \\ \left. - z \underline{k} \times \underline{r}_F + z \underline{k} \times \underline{r}_c \right]$$

$$= \frac{I}{L} \left[ (\underline{r}_a \times \underline{r}_D) + (\underline{r}_b \times \underline{r}_E) + (\underline{r}_c \times \underline{r}_F) + z \underline{k} \times (\underline{r}_a + \underline{r}_b + \underline{r}_c) \right. \\ \left. - z \underline{k} \times (\underline{r}_D + \underline{r}_E + \underline{r}_F) \right]$$

$$= \frac{I}{L} \left[ (\underline{r}_a \times \underline{r}_D) + (\underline{r}_b \times \underline{r}_E) + (\underline{r}_c \times \underline{r}_F) + z \underline{k} \times 3z \underline{k}^0 \right. \\ \left. - z \underline{k} \times 3L \underline{k} \right] \quad \text{--- (*)}$$

$$\underline{r}_a \times \underline{r}_D = \begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ R \cos \theta & R \sin \theta & z \\ R & 0 & L \end{vmatrix} = R L \sin \theta \underline{i} - R (L \cos \theta - z) \underline{j} \\ + R^2 \sin \theta \underline{k}$$

Since the LHS of the above equation (\*) has only  $\underline{k}$ , we need to consider only the  $\underline{k}$  component on RHS.

$$\underline{r}_b \times \underline{r}_E = \begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ R \cos\left(\frac{2\pi}{3} + \theta\right) & R \sin\left(\frac{2\pi}{3} + \theta\right) & Z \\ R \cos\left(\frac{2\pi}{3}\right) & R \sin\left(\frac{2\pi}{3}\right) & L \end{vmatrix}$$

$$= \underline{i} \left( R^2 \cos\left(\frac{2\pi}{3} + \theta\right) \sin\frac{2\pi}{3} - R^2 \sin\left(\frac{2\pi}{3} + \theta\right) \cos\frac{2\pi}{3} \right)$$

$$- \underline{j} \left( LR \cos\left(\frac{2\pi}{3} + \theta\right) - RZ \cos\frac{2\pi}{3} \right) + \underline{k} \left( R^2 \cos\left(\frac{2\pi}{3} + \theta\right) \sin\frac{2\pi}{3} - R^2 \sin\left(\frac{2\pi}{3} + \theta\right) \cos\frac{2\pi}{3} \right)$$

$$- \underline{k} R^2 \sin\theta$$

(using the identity:  $\sin(x+y) = \sin x \cos y + \cos x \sin y$ )

Similarly

$$\underline{r}_e \times \underline{r}_F = \underline{i} \left[ R^2 \cos\left(\frac{4\pi}{3} + \theta\right) \sin\frac{4\pi}{3} - R^2 \sin\left(\frac{4\pi}{3} + \theta\right) \cos\frac{4\pi}{3} \right]$$

$$- \underline{j} \left[ LR \cos\left(\frac{4\pi}{3} + \theta\right) - RZ \cos\frac{4\pi}{3} \right] + \underline{k} \left[ R^2 \cos\left(\frac{4\pi}{3} + \theta\right) \sin\frac{4\pi}{3} - R^2 \sin\left(\frac{4\pi}{3} + \theta\right) \cos\frac{4\pi}{3} \right]$$

$$- \underline{k} R^2 \sin\theta$$

You can verify that the sum of the  $\underline{i}$  components and  $\underline{j}$  components add up to zero.

$$\Rightarrow I \frac{d^2\theta}{dt^2} = (-3R^2 \sin\theta) \frac{T}{L} \Rightarrow \boxed{I \frac{d^2\theta}{dt^2} + \frac{3R^2 T}{L} \sin\theta = 0}$$

(j) For small values of  $\theta$ ,  $\sin\theta \approx \theta$

$$\Rightarrow \omega_n = \sqrt{\frac{3R^2T}{IL}} \quad \text{--- *}$$

(k) Let's call the time period from (j) above, ie

$$\text{the approximate time period } T_{app} = \frac{2\pi}{\omega_n} = \frac{2\pi}{\sqrt{\frac{3R^2T}{IL}}} \quad (2)$$

Now, we can calculate the actual time period ( $T_{real}$ ) for a given value of  $\theta_0$  by solving the eom (1) with MATLAB. To write MATLAB code, we need numerical values for  $R, T, I, L$ . We can proceed in one of 2 ways.

(i) Assume arbitrary values for  $R, T, I, L, \dots$

Get  $T_{app}$  from eq (2) above

Solve EOM with MATLAB

$$\frac{d}{dt} \begin{bmatrix} \theta \\ \omega \end{bmatrix} = \begin{bmatrix} \omega \\ -\frac{3R^2T}{IL} \sin\theta \end{bmatrix}, \text{ Initial conditions } [\theta_0, 0]$$

Get  $T_{real}$  as a function of  $\theta_0$ .

Find the range of  $\theta_0$  for which  $T_{app} & T_{real}$  are within 5% and 1% of each other.

ii) Alternatively, we can eliminate the physical parameters by normalizing the time as

$\tau = \frac{t}{T_{app}}$ . Then the EOM becomes

$$\frac{1}{T_{app}^2} \frac{d^2\theta}{d\tau^2} + \frac{4\pi^2}{T_{app}^2} \sin\theta = 0 \Rightarrow \boxed{\frac{d^2\theta}{d\tau^2} + 4\pi^2 \sin\theta = 0}$$

This equation is now in terms of non-dimensional quantities only. Linearize it :  $\frac{d^2\theta}{d\tau^2} + 4\pi^2\theta = 0$

$\Rightarrow$  Approximate time period  $T_{app} = 1$

Use MATLAB to find  $T_{real}$  as a function of  $\theta_0$ .

Find the range of  $\theta_0$  for which  $T_{app}$  &  $T_{real}$  are within 5% & 1% of each other.

For 5% error,  $\theta_0 = 0.8692$  radians

for 1% error,  $\theta_0 = 0.3979$  radians

```

function hw7problem3
    close all;

    % write a for loop to solve the equation of motion (eom) for
    different
    % values of theta_0 between 0 and pi/3.
    for i=1:100
        theta0(i)=pi/3*i/100;
        ic=[theta0(i),0];
        options=odeset('Event',@detect_zero_crossing);
        [t,w,tevent,wevent,index]=ode45(@eom,[0,5],ic,options);
        % time difference between two successive events is t_real
        t_real(i)=tevent(3)-tevent(2);
    end

    plot(theta0,t_real)

    % following is the code to detect the range of theta_0 for which
    % t_real is within 5% and 1% of t_app

    for i=1:100
        if (t_real(i)<1.05)
            theta0_5=theta0(i);
        end
        if (t_real(i)<1.01)
            theta0_1=theta0(i);
        end
    end

    % write the values of theta_0 for 5% error adn 1% error to the
    screen.
    theta0_5
    theta0_1

    % function of the eom in terms of the normalized time "tau"
    function dwdt=eom(t,w)
        dwdt=[w(2);-4*pi^2*sin(w(1))];
    end

    % event function to detect when theta crosses zero with positive
    slope
    function [value,stop,dir]=detect_zero_crossing(t,w)
        value=w(1);
        stop=0;
        dir=1;
    end

end

```

